Presented by Erik C. Baker

This program extends the 1986 VPM algorithm (Yount & Hoffman) to include mixed gas, repetitive, and altitude diving. Developments to the algorithm were made by David E. Yount, Eric B. Maiken, and Erik C. Baker over a period from 1999 to 2001.

This work is dedicated in remembrance of Professor David E. Yount who passed away on April 27, 2000.

Distribute freely - credit the authors.

Introductory Notes:

- This paper includes an explanation about the program settings and the altitude dive algorithm settings, a sample input file format, a sample program output, and the program code in Fortran. The intent is that readers will be able to port the code to the programming language and operating platform of their choice. This program does not include the coding for a graphical user interface that is left for the users to implement.
- 2. While there are some similarities to Haldanian decompression algorithms in this program, there are many differences. Ascent ceilings are determined based on allowable gradients for bubble formation rather than M-values. These supersaturation gradients are determined by tracking sets of VPM nuclei (bubble seeds) of a certain initial critical radius. These are the microscopic physical structures that stabilize free-phase gas and that can grow into full-fledged bubbles when the supersaturation gradient is sufficient to probe the Laplace condition for bubble formation.
- 3. VPM ascent profiles are characteristically different than Haldanian ascent profiles. Most notable is that deeper initial stops are required in the profiles and typically less time is required at the shallow stops. The conclusion to be drawn from this is that if you don't allow many bubbles to form in the early portion of the ascent profile, you won't have to spend as much time in the latter portion resolving bubbles.
- 4. There are two options for the determination of allowable gradients a constant bubble number approach and a dynamic critical volume approach. This program will compute either depending on whether the Critical Volume Algorithm is toggled on or off. If it is off then a fixed constant bubble number gradient determines the ascent profile. If it is on then the algorithm will relax the allowable gradients, deliberately allowing some bubbles to form, as long the amount of excess released-gas does not exceed a predetermined critical volume (this limit is set by the Critical Volume Parameter Lambda). The Critical Volume Algorithm will have the most noticeable effect for short dives in the no-deco range, but very little effect for long decompression dives. Users simply need to work with the algorithm for a while to develop an understanding of its behavior.

<u>VPM Program Settings in the file VPMDECO.SET:</u>

```
&Program Settings
Units='fsw'
                                            !Options: fsw or msw
Altitude Dive Algorithm='OFF'
                                            !Options: ON or OFF
Minimum Deco Stop Time=1.0
                                            !Options: real positive number
Critical Radius N2 Microns=0.8
                                            !Adj. Range: 0.2 to 1.35 microns
Critical Radius He Microns=0.7
                                            !Adj. Range: 0.2 to 1.35 microns
Critical Volume Algorithm='ON'
                                            !Options: ON or OFF
Crit Volume Parameter Lambda=7500.0
                                            !Adj. Range: 6500 to 8300 fsw-min
Gradient Onset of Imperm Atm=8.2
                                            !Adj. Range: 5.0 to 10.0 atm
Surface Tension Gamma=0.0179
                                           !Adj. Range: 0.015 to 0.065 N/m
Skin Compression GammaC=0.257
                                          !Adj. Range: 0.160 to 0.290 N/m
                                        !Adj. Range: 10080 to 51840 min
!Constant value for PO2 up to 2 atm
Regeneration_Time_Constant=20160.0
Pressure Other Gases mmHg=102.0
```

Notes:

- 5. Adjustability range for Critical Radii according to research by Yount and colleagues. DEFAULT VALUES ARE 0.8 FOR NITROGEN AND 0.7 FOR HELIUM. For dives involving exertion, cold water, dehydration, diver in poor or fair physical conditioning, or other predisposing factors to DCS, the critical radii should adjusted upwards to 1.0 for nitrogen/0.9 for helium (moderate conservatism) or 1.2 for nitrogen/1.1 for helium (heavy conservatism). Values below the defaults should only be used by skilled divers in good or excellent physical conditioning, with no predisposing factors to DCS, and after several work-up dives decreasing the values in small increments to verify suitability of the lower values.
- 6. Adjustability range for Critical Volume Parameter Lambda according to Wienke. DEFAULT VALUE IS 7500 FSW-MIN. This applies whether the program is set to fsw units or msw units. Conversion to Pascals-min for calculations will be made automatically by the program.
- 7. Adjustability range for Gradient for Onset of Impermeability according to research by Yount and Hoffman. DEFAULT VALUE IS 8.2 ATMOSPHERES (this is a pressure gradient value, not an absolute pressure). It should be noted that Yount and Hoffman reduced the value to 5.0 atm for helium (heliox) dives. A lower number will make the deco profiles more conservative.
- 8. Adjustability ranges for Surface Tension Gamma and Skin Compression GammaC according to Wienke. DEFAULT VALUES ARE 0.0179 GAMMA AND 0.257 GAMMAC (based on research by Yount and colleauges).
- 9. Adjustability range for Regeneration Time Constant according to Wienke. DEFAULT VALUE IS 20160 (this is equal to 2 weeks, the value used by Yount and Hoffman).
- 10. Constant pressure for other gases oxygen, carbon dioxide, and water vapor according to Yount and Lally. This is supposedly valid for partial pressures of oxygen up to 2.0 atmospheres absolute which would contain all the typical exposures for technical diving. The value is given in millimeters of mercury based on the original research, however it is automatically converted to the proper pressure units in the program, whether set to fsw units or msw units.

VPM Altitude Dive Algorithm Settings in the file ALTITUDE.SET:

```
&Altitude_Dive_Settings
Altitude_of_Dive=0 !Limit is 30,000 feet/9,144 meters
Diver_Acclimatized_at_Altitude='no' !Acclimatization takes 2 weeks+
Starting_Acclimatized_Altitude=0 !Altitude for 2 weeks+ before ascent
Ascent_to_Altitude_Hours=1 !Average ascent rate in hours
Hours_at_Altitude_Before_Dive=2 !Off-gassing is tracked
```

Notes:

- 1. Altitude of dive cannot be higher than Mount Everest!
- 2. If diver is not acclimatized to altitude, and makes ascent to altitude before the dive, critical radii and gas loadings in the half-time compartments will be adjusted accordingly.
- 3. Average ascent rate to altitude is based on driving in a vehicle. For quick flights to the dive site at altitude, the average ascent rate might be much more rapid, as in tenths of an hour.

Sample input file format from the file VPMDECO.IN:

```
TRIMIX DIVE TO 260 FSW
                              !Description of dive
                        !Number of gas mixes
.15,.45,.40
                              !Fraction O2, Fraction He, Fraction N2
.36,.00,.64
                              !Fraction O2, Fraction He, Fraction N2
1.0,.00,.00
                              !Fraction O2, Fraction He, Fraction N2
                        !Profile code 1 = descent
0,260,75,1
                              !Starting depth, ending depth, rate, gasmix
                        !Profile code 2 = constant depth
260,30,1
                        !Depth, run time at end of segment, gasmix
                        !Profile code 99 = decompress
99
                        !Number of ascent parameter changes
                              !Starting depth, gasmix, rate, step size
260,1,-30,10
110,2,-30,10
                              !Change depth, gasmix, rate, step size
20,3,-10,20
                              !Change depth, gasmix, rate, step size
                        !Repetitive code 1 = repetitive dive to follow
                        !Surface interval time in minutes
TRIMIX DIVE TO 260 FSW
                              !Description of dive
                        !Number of gas mixes
.15,.45,.40
                              !Fraction O2, Fraction He, Fraction N2
.36,.00,.64
                              !Fraction O2, Fraction He, Fraction N2
1.0,.00,.00
                              !Fraction O2, Fraction He, Fraction N2
                        !Profile code 1 = descent
0,260,75,1
                              !Starting depth, ending depth, rate, gasmix
                        !Profile code 2 = constant depth
260,30,1
                        !Depth, run time at end of segment, gasmix
99
                        !Profile code 99 = decompress
                        !Number of ascent parameter changes
260,1,-30,10
                              !Starting depth, gasmix, rate, step size
                              !Change depth, gasmix, rate, step size
110,2,-30,10
20,3,-10,20
                              !Change depth, gasmix, rate, step size
                        !Repetitive code 0 = last dive/end of file
```

Sample output from the file VPMDECO.OUT:

!using default program settings

DECOMPRESSION CALCULATION PROGRAM Developed in FORTRAN by Erik C. Baker

Program Run: 04-09-2001 at 09:02 pm Model: VPM 2001

Description: TRIMIX DIVE TO 260 FSW

FHe Gasmix Summary: FO2 FN2 Gasmix # 1 .150 .450 .400 .640 .360

Gasmix # 2 .360 .000 Gasmix # 3 1.000 .000 .000

DIVE PROFILE

Seg- ment #	Segm. Time (min)	Run Time (min)	Gasmix Used #	or	From Depth (fswg)	To Depth (fswg)	Rate +Dn/-Up (fsw/min)	Constant Depth (fswg)
1 2	3.5	3.5	1 1 1	Descent	0.	260.	75.0	260.

DECOMPRESSION PROFILE

Leading compartment enters the decompression zone at 209.7 fswg Deepest possible decompression stop is 200.0 fswg

	Segm. Time	Run Time	Gasmix Used	Ascent To	Ascent Rate	Col Not	DECO STOP	STOP TIME	RUN TIME
#	(min)	(min)	#		(fsw/min)	:	(fswg)		(min)
3 4	2.7	32.7 33.0	1 1	180.	-30.0		180	1	33
4 5	.3	33.3	1 1	170.	-30.0		100	1	33
6	. 3 . 7	34.0	1	170.	-30.0		170	1	34
7	. 3	34.3	1 1	160.	-30.0	-	170	_	31
8	.7	35.0	1 1	100.	30.0	i	160	1	35
9	.3	35.3	1	150.	-30.0	İ		_	
10	1.7	37.0	1 1			İ	150	2	37
11	.3	37.3	1	140.	-30.0	İ			
12	1.7	39.0	1 1			İ	140	2	39
13	.3	39.3	1	130.	-30.0				
14	1.7	41.0	1				130	2	41
15	.3	41.3	1 1	120.	-30.0				
16	2.7	44.0	1				120	3	44
17	.3	44.3	1	110.	-30.0				
18	1.7	46.0	2	100	20.0		110	2	46
19	.3	46.3	2 2	100.	-30.0	-	1.00	1	47
20 21	.7 .3	47.0 47.3	2	90.	-30.0		100	1	47
22	1.7	49.0	2	90.	-30.0	-	90	2	49
23	.3	49.3	2	80.	-30.0	-	50	2	4.7
24	1.7	51.0	2	00.	30.0		80	2	51
25	.3	51.3	2	70.	-30.0	i			
26	2.7	54.0	2				70	3	54
27	.3	54.3	2	60.	-30.0	İ			
28	3.7	58.0	2			ĺ	60	4	58
29	.3	58.3	2	50.	-30.0				
30	4.7	63.0	2				50	5	63
31	.3	63.3	2	40.	-30.0	ļ			
32	5.7	69.0	2				40	6	69
33	.3 7.7	69.3	2	30.	-30.0		30	8	77
34		77.0	2	20.	20.0		30	8	77
35 36	.3 21.7	77.3 99.0	2 3	∠∪.	-30.0		20	22	99
37	21.7	101.0	3	0.	-10.0	-	20	44	ט ט
5 /	2.0	101.0	1 5 1	0.	10.0	ı			

REPETITIVE DIVE:

!Surface interval = 60 min

DECOMPRESSION CALCULATION PROGRAM Developed in FORTRAN by Erik C. Baker

Program Run: 04-09-2001 at 09:02 pm Model: VPM 2001

Description: TRIMIX DIVE TO 260 FSW

Gasmix Summary: FO2 FHe FN2
Gasmix # 1 .150 .450 .400
Gasmix # 2 .360 .000 .640
Gasmix # 3 1.000 .000

DIVE PROFILE

Seg-	Segm.	Run	Gasmix	Ascent	From	To	Rate	Constant
ment	Time	Time	Used	or	Depth	Depth	+Dn/-Up	Depth
#	(min)	(min)	#	Descent	(fswg)	(fswg)	(fsw/min)	(fswg)
1	3.5	3.5	1	Descent	0.	260.	75.0	
2	26.5	30.0	1	İ				260.

DECOMPRESSION PROFILE

Leading compartment enters the decompression zone at 209.7 fswg Deepest possible decompression stop is 200.0 fswg

Seg- ment #	Segm. Time (min)	Run Time (min)	Gasmix Used #	То	Ascent Rate (fsw/min)	Col Not Used	DECO STOP (fswg)	STOP TIME (min)	RUN TIME (min)
3	2.7	32.7	1	180.	-30.0				
4	.3	33.0	1				180	1	33
5	.3	33.3	1	170.	-30.0				
6	.7	34.0	1				170	1	34
7	.3	34.3	1	160.	-30.0				
8	1.7	36.0	1				160	2	36
9	.3	36.3	1	150.	-30.0				
10	. 7	37.0	1 1				150	1	37
11	.3	37.3	1	140.	-30.0				
12	1.7	39.0	1				140	2	39
13	.3	39.3	1	130.	-30.0				
14	1.7	41.0	1				130	2	41
15	.3	41.3	1	120.	-30.0				
16	2.7	44.0	1				120	3	44
17	.3	44.3	1	110.	-30.0				
18	1.7	46.0	2				110	2	46
19	.3	46.3	2	100.	-30.0				
20	. 7	47.0	2				100	1	47
21	.3	47.3	2	90.	-30.0				
22	1.7	49.0	2				90	2	49
23	.3	49.3	2	80.	-30.0				
24	2.7	52.0	2				80	3	52
25	.3	52.3	2	70.	-30.0			_	
26	3.7	56.0	2				70	4	56
27	.3	56.3	2	60.	-30.0		60		6.0
28	3.7	60.0	2		2.0		60	4	60
29	.3	60.3	2	50.	-30.0		F 0	-	6.77
30	6.7	67.0	2 2	1 40	20.0		50	7	67
31	.3	67.3		40.	-30.0		4.0	0	7.0
32 33	8.7	76.0	2 2	30.	-30.0		40	9	76
		76.3] 30.	-30.0		2.0	12	0.0
34 35	11.7 .3	88.0 88.3	2 2	20.	-30.0		30	12	88
35 36	. <i>3</i> 35.7	124.0	3	, 20.	-30.0		20	36	124
37	2.0	124.0	3	0.	-10.0		20	30	124

Varying Permeability Model (VPM) Decompression Program in Fortran PROGRAM VPMDECO C Varying Permeability Model (VPM) Decompression Program in FORTRAN С С Author: Erik C. Baker C С "DISTRIBUTE FREELY - CREDIT THE AUTHORS" С С This program extends the 1986 VPM algorithm (Yount & Hoffman) to include C mixed gas, repetitive, and altitude diving. Developments to the algorithm С were made by David E. Yount, Eric B. Maiken, and Erik C. Baker over a С period from 1999 to 2001. This work is dedicated in remembrance of C C CProfessor David E. Yount who passed away on April 27, 2000. Notes: 1. This program uses the sixteen (16) half-time compartments of the C Buhlmann ZH-L16 model. The optional Compartment 1b is used here with С half-times of 1.88 minutes for helium and 5.0 minutes for nitrogen. С С 2. This program uses various DEC, IBM, and Microsoft extensions which С may not be supported by all FORTRAN compilers. Comments are made with C a capital "C" in the first column or an exclamation point "!" placed C in a line after code. An asterisk "*" in column 6 is a continuation of the previous line. All code, except for line numbers, starts in C С column 7. С С 3. Comments and suggestions for improvements are welcome. Please С respond by e-mail to: EBaker@se.aeieng.com С С Acknowledgment: Thanks to Kurt Spaugh for recommendations on how to clean up the code. IMPLICIT NONE LOCAL VARIABLES - MAIN PROGRAM CHARACTER M*1, OS Command*3, Word*7, Units*3 CHARACTER Line1*70, Critical Volume Algorithm*3 CHARACTER Units Word1*4, Units Word2*7, Altitude Dive Algorithm*3 INTEGER I, J !loop counters INTEGER*2 Month, Day, Year, Clock Hour, Minute INTEGER Number of Mixes, Number of Changes, Profile Code INTEGER Segment Number Start of Ascent, Repetitive Dive Flag LOGICAL Schedule Converged, Critical Volume Algorithm Off LOGICAL Altitude Dive Algorithm Off REAL Deco Ceiling Depth, Deco Stop Depth, Step Size REAL Sum_of_Fractions, Sum_Check REAL Depth, Ending_Depth, Starting_Depth REAL Rate, Rounding Operation1, Run Time End of Segment REAL Last Run Time, Stop Time, Depth Start of Deco Zone

REAL Rounding Operation2, Deepest Possible Stop Depth

REAL First_Stop_Depth, Critical_Volume_Comparison

REAL Next Stop, Run Time Start of Deco Zone

REAL Critical Radius N2 Microns, Critical Radius He Microns

REAL Run Time Start of Ascent, Altitude of Dive

REAL Deco_Phase_Volume_Time, Surface_Interval_Time

REAL Pressure Other Gases mmHg

C LOCAL ARRAYS - MAIN PROGRAM

INTEGER Mix Change(10)

```
REAL Fraction Oxygen(10)
    REAL Depth Change (10)
    REAL Rate_Change(10), Step_Size_Change(10)
    REAL Helium_Half_Time(16), Nitrogen_Half_Time(16)
    REAL He_Pressure_Start_of_Ascent(16)
    REAL N2_Pressure_Start_of_Ascent(16)
    REAL He Pressure Start of Deco Zone (16)
    REAL N2 Pressure Start of Deco Zone (16)
    REAL Phase Volume Time (16)
    REAL Last Phase Volume Time (16)
GLOBAL CONSTANTS IN NAMED COMMON BLOCKS
REAL Water Vapor Pressure
    COMMON /Block 8/ Water Vapor Pressure
    REAL Surface Tension Gamma, Skin Compression GammaC
    COMMON /Block_19/ Surface_Tension_Gamma, Skin_Compression_GammaC
    REAL Crit Volume Parameter Lambda
    COMMON /Block 20/ Crit Volume Parameter Lambda
    REAL Minimum Deco_Stop_Time
    COMMON /Block 21/ Minimum Deco Stop Time
    REAL Regeneration_Time_Constant
    COMMON /Block 22/ Regeneration Time Constant
    REAL Constant Pressure Other Gases
    COMMON /Block 17/ Constant Pressure Other Gases
    REAL Gradient Onset of Imperm Atm
    COMMON /Block 14/ Gradient Onset of Imperm Atm
GLOBAL VARIABLES IN NAMED COMMON BLOCKS
INTEGER Segment Number
    REAL Run Time, Segment Time
    COMMON /Block 2/ Run Time, Segment Number, Segment Time
    REAL Ending Ambient Pressure
    COMMON /Block 4/ Ending Ambient Pressure
    INTEGER Mix Number
    COMMON /Block 9/ Mix Number
    REAL Barometric Pressure
    COMMON /Block_18/ Barometric_Pressure
    LOGICAL Units Equal Fsw, Units Equal Msw
    COMMON /Block 15/ Units Equal Fsw, Units Equal Msw
    REAL Units Factor
    COMMON /Block 16/ Units Factor
GLOBAL ARRAYS IN NAMED COMMON BLOCKS
REAL Helium Time Constant (16)
    COMMON /Block 1A/ Helium Time Constant
    REAL Nitrogen Time Constant (16)
    COMMON /Block 1B/ Nitrogen Time Constant
    REAL Helium Pressure (16), Nitrogen Pressure (16)
```

```
COMMON /Block 3/ Helium Pressure, Nitrogen Pressure
         REAL Fraction Helium(10), Fraction Nitrogen(10)
         COMMON /Block 5/ Fraction Helium, Fraction Nitrogen
         REAL Initial Critical Radius He(16)
         REAL Initial Critical Radius N2(16)
         COMMON /Block 6/ Initial Critical Radius He,
                          Initial Critical Radius N2
         REAL Adjusted Critical Radius He(16)
         REAL Adjusted Critical Radius N2 (16)
         COMMON /Block 7/ Adjusted Critical Radius He,
                          Adjusted Critical Radius N2
         REAL Max Crushing Pressure He(16), Max Crushing Pressure N2(16)
         COMMON /Block 10/ Max Crushing Pressure He,
                                     Max_Crushing_Pressure N2
         REAL Surface Phase Volume Time (16)
         COMMON /Block 11/ Surface Phase Volume Time
         REAL Max Actual Gradient (16)
         COMMON /Block 12/ Max Actual Gradient
         REAL Amb Pressure Onset of Imperm(16)
         REAL Gas Tension Onset of Imperm(16)
         COMMON /Block 13/ Amb Pressure Onset of Imperm,
                          Gas Tension Onset of Imperm
NAMELIST FOR PROGRAM SETTINGS (READ IN FROM ASCII TEXT FILE)
NAMELIST / Program Settings / Units, Altitude Dive Algorithm,
                      Minimum Deco Stop Time, Critical Radius N2 Microns,
                       Critical Radius He Microns, Critical Volume Algorithm,
                       Crit Volume Parameter Lambda,
                       Gradient Onset of Imperm Atm,
                       Surface Tension Gamma, Skin Compression GammaC,
                       Regeneration Time Constant, Pressure Other Gases mmHg
ASSIGN HALF-TIME VALUES TO BUHLMANN COMPARTMENT ARRAYS
DATA Helium_Half_Time(1)/1.88/,Helium_Half_Time(2)/3.02/,

* Helium_Half_Time(3)/4.72/,Helium_Half_Time(4)/6.99/,
                 \label{eq:helium_Half_Time(5)/10.21/, Helium_Half_Time(6)/14.48/, Helium_Half_Time(7)/20.53/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8)/29.11/, Helium_Half_Time(8
                 Helium_Half_Time(9)/41.20/,Helium_Half_Time(10)/55.19/,
                 Helium_Half_Time(11)/70.69/,Helium_Half_Time(12)/90.34/,
                 Helium_Half_Time(13)/115.29/, Helium_Half_Time(14)/147.42/,
                 Helium Half Time (15) /188.24/, Helium Half Time (16) /240.03/
         DATA Nitrogen_Half_Time(1)/5.0/,Nitrogen_Half_Time(2)/8.0/,
                 Nitrogen Half Time(3)/12.5/, Nitrogen Half Time(4)/18.5/,
                 Nitrogen Half Time(5)/27.0/, Nitrogen Half Time(6)/38.3/,
                 Nitrogen Half Time(7)/54.3/, Nitrogen Half Time(8)/77.0/,
                 Nitrogen Half Time (9)/109.0/, Nitrogen Half Time (10)/146.0/,
                 Nitrogen Half Time (11) /187.0/, Nitrogen Half Time (12) /239.0/,
                 Nitrogen Half Time(13)/305.0/, Nitrogen Half Time(14)/390.0/,
                 Nitrogen Half Time (15) /498.0/, Nitrogen Half Time (16) /635.0/
OPEN FILES FOR PROGRAM INPUT/OUTPUT
OPEN (UNIT = 7, FILE = 'VPMDECO.IN', STATUS = 'UNKNOWN',
                      ACCESS = 'SEQUENTIAL', FORM = 'FORMATTED')
         OPEN (UNIT = 8, FILE = 'VPMDECO.OUT', STATUS = 'UNKNOWN',
```

```
ACCESS = 'SEQUENTIAL', FORM = 'FORMATTED')
     OPEN (UNIT = 10, FILE = 'VPMDECO.SET', STATUS = 'UNKNOWN',
    * ACCESS = 'SEQUENTIAL', FORM = 'FORMATTED')
BEGIN PROGRAM EXECUTION WITH OUTPUT MESSAGE TO SCREEN
OS Command = 'CLS'
     CALL SYSTEMQQ (OS Command)
                                            !Pass "clear screen" command
     PRINT *,''
                                            !to MS operating system
     PRINT *, 'PROGRAM VPMDECO'
     PRINT *,''
                                     !asterisk indicates print to screen
READ IN PROGRAM SETTINGS AND CHECK FOR ERRORS
    IF THERE ARE ERRORS, WRITE AN ERROR MESSAGE AND TERMINATE PROGRAM
READ (10, Program Settings)
     IF ((Units .EQ. 'fsw').OR.(Units .EQ. 'FSW')) THEN
        Units Equal Fsw = (.TRUE.)
        Units Equal Msw = (.FALSE.)
     ELSE IF ((Units .EQ. 'msw').OR.(Units .EQ. 'MSW')) THEN
        Units_Equal_Fsw = (.FALSE.)
        Units Equal Msw = (.TRUE.)
     ELSE
        CALL SYSTEMQQ (OS Command)
        WRITE (*,901)
        WRITE (*,900)
        STOP 'PROGRAM TERMINATED'
     END IF
     IF ((Altitude Dive Algorithm .EQ. 'ON') .OR.
                          (Altitude Dive Algorithm .EQ. 'on')) THEN
        Altitude Dive Algorithm Off = (.FALSE.)
     ELSE IF ((Altitude Dive Algorithm .EQ. 'OFF') .OR.
                         (Altitude Dive Algorithm .EQ. 'off')) THEN
        Altitude Dive Algorithm Off = (.TRUE.)
     ELSE
        WRITE (*,902)
        WRITE (*,900)
        STOP 'PROGRAM TERMINATED'
     END IF
     IF ((Critical Radius N2 Microns .LT. 0.2) .OR.
        (Critical Radius N2 Microns .GT. 1.35)) THEN
        CALL SYSTEMQQ (OS Command)
        WRITE (*,903)
        WRITE (*,900)
        STOP 'PROGRAM TERMINATED'
     END IF
     IF ((Critical_Radius_He_Microns .LT. 0.2) .OR.
        (Critical Radius He Microns .GT. 1.35)) THEN
        CALL SYSTEMQQ (OS Command)
        WRITE (*,903)
        WRITE (*,900)
        STOP 'PROGRAM TERMINATED'
     END IF
     IF ((Critical Volume Algorithm .EQ. 'ON').OR.
                        (Critical Volume Algorithm .EQ. 'on')) THEN
        Critical Volume Algorithm Off = (.FALSE.)
     ELSE IF ((Critical Volume Algorithm .EQ. 'OFF').OR.
                        (Critical Volume Algorithm .EQ. 'off')) THEN
        Critical Volume Algorithm Off = (.TRUE.)
```

```
ELSE
        WRITE (*,904)
        WRITE (*,900)
        STOP 'PROGRAM TERMINATED'
    END IF
INITIALIZE CONSTANTS/VARIABLES BASED ON SELECTION OF UNITS - FSW OR MSW
C
    fsw = feet of seawater, a unit of pressure
    msw = meters of seawater, a unit of pressure
IF (Units Equal Fsw) THEN
        WRITE (*,800)
        Units Word1 = 'fswg'
        Units Word2 = 'fsw/min'
        Units Factor = 33.0
        Water_Vapor_Pressure = 1.607 !based on respiratory quotient of 0.8
                                   ! (Schreiner value)
    END IF
     IF (Units Equal Msw) THEN
        WRITE (*,801)
        Units Word1 = 'mswg'
        Units Word2 = 'msw/min'
        Units Factor = 10.1325
        Water Vapor Pressure = 0.493
                                   !based on respiratory quotient of 0.8
    END IF
                                   ! (Schreiner value)
INITIALIZE CONSTANTS/VARIABLES
Constant Pressure Other Gases = (Pressure Other Gases mmHg/760.0)
                               * Units Factor
    Run Time = 0.0
    Segment Number = 0
    DO I = 1,16
         Helium Time Constant(I) = ALOG(2.0)/Helium Half Time(I)
         Nitrogen Time Constant(I) = ALOG(2.0)/Nitrogen Half Time(I)
         Max Crushing Pressure He(I) = 0.0
         Max Crushing Pressure N2(I) = 0.0
         Max Actual Gradient(I) = 0.0
         Surface Phase Volume Time(I) = 0.0
         Amb_Pressure_Onset_of_Imperm(I) = 0.0
Gas_Tension_Onset_of_Imperm(I) = 0.0
         Initial Critical_Radius_N2(I) = Critical_Radius_N2_Microns
         Initial_Critical_Radius_He(I) = Critical_Radius_He_Microns
    END DO
INITIALIZE VARIABLES FOR SEA LEVEL OR ALTITUDE DIVE
С
    See subroutines for explanation of altitude calculations. Purposes are
С
    1) to determine barometric pressure and 2) set or adjust the VPM critical
C
    radius variables and gas loadings, as applicable, based on altitude,
    ascent to altitude before the dive, and time at altitude before the dive
IF (Altitude Dive Algorithm Off) THEN
        Altitude of Dive = 0.0
        CALL CALC BAROMETRIC PRESSURE (Altitude of Dive)
                                                        !subroutine
        WRITE (*,802) Altitude of Dive, Barometric Pressure
        DO I = 1,16
        Adjusted Critical Radius N2(I) = Initial Critical Radius N2(I)
        Adjusted Critical Radius He(I) = Initial Critical Radius He(I)
        Helium Pressure(I) = 0.0
        Nitrogen Pressure(I) = (Barometric Pressure -
           Water Vapor Pressure) *0.79
```

```
END DO
     ELSE
        CALL VPM ALTITUDE DIVE ALGORITHM
                                                          !subroutine
    END IF
START OF REPETITIVE DIVE LOOP
    This is the largest loop in the main program and operates between Lines
    30 and 330. If there is one or more repetitive dives, the program will
    return to this point to process each repetitive dive.
30 DO 330, WHILE (.TRUE.)
                                 !loop will run continuously until
                                      !there is an exit statement
INPUT DIVE DESCRIPTION AND GAS MIX DATA FROM ASCII TEXT INPUT FILE
    BEGIN WRITING HEADINGS/OUTPUT TO ASCII TEXT OUTPUT FILE
    See separate explanation of format for input file.
C-----
    READ (7,805) Line1
    CALL CLOCK (Year, Month, Day, Clock Hour, Minute, M)
    WRITE (8,810)
    WRITE (8,811)
    WRITE (8,812)
    WRITE (8,813)
    WRITE (8,813)
    WRITE (8,814) Month, Day, Year, Clock Hour, Minute, M
    WRITE (8,813)
    WRITE (8,815) Line1
    WRITE (8,813)
    READ (7,*) Number of Mixes
                                           !check for errors in gasmixes
    DO I = 1, Number of Mixes
        READ (7,*) Fraction Oxygen(I), Fraction Helium(I),
                 Fraction Nitrogen(I)
        Sum of Fractions = Fraction Oxygen(I) + Fraction Helium(I) +
                        Fraction Nitrogen(I)
        Sum Check = Sum of Fractions
        IF (Sum Check .NE. 1.0) THEN
           CALL SYSTEMQQ (OS Command)
           WRITE (*,906)
           WRITE (*,900)
           STOP 'PROGRAM TERMINATED'
        END IF
    END DO
    WRITE (8,820)
    DO J = 1, Number of Mixes
        WRITE (8,821) J, Fraction_Oxygen(J), Fraction_Helium(J),
                      Fraction Nitrogen (J)
    END DO
    WRITE (8,813)
    WRITE (8,813)
    WRITE (8,830)
    WRITE (8,813)
    WRITE (8,831)
    WRITE (8,832)
    WRITE (8,833) Units Word1, Units Word1, Units Word2, Units Word1
    WRITE (8,834)
DIVE PROFILE LOOP - INPUT DIVE PROFILE DATA FROM ASCII TEXT INPUT FILE
    AND PROCESS DIVE AS A SERIES OF ASCENT/DESCENT AND CONSTANT DEPTH
    SEGMENTS. THIS ALLOWS FOR MULTI-LEVEL DIVES AND UNUSUAL PROFILES. UPDATE
    GAS LOADINGS FOR EACH SEGMENT. IF IT IS A DESCENT SEGMENT, CALC CRUSHING
    PRESSURE ON CRITICAL RADII IN EACH COMPARTMENT.
C
    "Instantaneous" descents are not used in the VPM. All ascent/descent
С
    segments must have a realistic rate of ascent/descent. Unlike Haldanian
    models, the VPM is actually more conservative when the descent rate is
```

```
slower becuase the effective crushing pressure is reduced. Also, a
    realistic actual supersaturation gradient must be calculated during
C
    ascents as this affects critical radii adjustments for repetitive dives.
    Profile codes: 1 = Ascent/Descent, 2 = Constant Depth, 99 = Decompress
DO WHILE (.TRUE.)
                                     !loop will run continuously until
                                     !there is an exit statement
    READ (7,*) Profile Code
    IF (Profile Code .EQ. 1) THEN
       READ (7,*) Starting Depth, Ending Depth, Rate, Mix Number
        CALL GAS LOADINGS ASCENT DESCENT (Starting Depth,
                                                       !subroutine
                                   Ending Depth, Rate)
        IF (Ending Depth .GT. Starting Depth) THEN
           CALL CALC CRUSHING PRESSURE (Starting Depth,
                                                      !subroutine
                                  Ending Depth, Rate)
        END IF
        IF (Ending Depth .GT. Starting Depth) THEN
           Word = 'Descent'
        ELSE IF (Starting Depth .GT. Ending Depth) THEN
           Word = 'Ascent '
        ELSE
           Word = 'ERROR'
        END IF
        WRITE (8,840) Segment Number, Segment Time, Run Time,
                   Mix Number, Word, Starting Depth, Ending Depth,
                   Rate
    ELSE IF (Profile Code .EQ. 2) THEN
       READ (7,*) Depth, Run Time End of Segment, Mix Number
        CALL GAS LOADINGS CONSTANT DEPTH (Depth,
                                                       !subroutine
                                   Run Time End of Segment)
       WRITE (8,845) Segment Number, Segment Time, Run Time,
                   Mix Number, Depth
    ELSE IF (Profile Code .EQ. 99) THEN
       EXIT
    ELSE
        CALL SYSTEMQQ (OS Command)
        WRITE (*,907)
        WRITE (*,900)
        STOP 'PROGRAM TERMINATED'
    END IF
    END DO
BEGIN PROCESS OF ASCENT AND DECOMPRESSION
    First, calculate the regeneration of critical radii that takes place over
    the dive time. The regeneration time constant has a time scale of weeks
    so this will have very little impact on dives of normal length, but will
    have major impact for saturation dives.
CALL NUCLEAR REGENERATION (Run Time)
                                                       !subroutine
CALCULATE INITIAL ALLOWABLE GRADIENTS FOR ASCENT
C
    This is based on the maximum effective crushing pressure on critical radii
    in each compartment achieved during the dive profile.
CALL CALC INITIAL ALLOWABLE GRADIENT
SAVE VARIABLES AT START OF ASCENT (END OF BOTTOM TIME) SINCE THESE WILL
    BE USED LATER TO COMPUTE THE FINAL ASCENT PROFILE THAT IS WRITTEN TO THE
    OUTPUT FILE.
    The VPM uses an iterative process to compute decompression schedules so
    there will be more than one pass through the decompression loop.
```

```
DO I = 1,16
        He Pressure Start of Ascent(I) = Helium Pressure(I)
         N2 Pressure Start of Ascent(I) = Nitrogen Pressure(I)
     END DO
     Run Time Start of Ascent = Run Time
     Segment Number Start of Ascent = Segment Number
INPUT PARAMETERS TO BE USED FOR STAGED DECOMPRESSION AND SAVE IN ARRAYS.
C
С
     ASSIGN INITAL PARAMETERS TO BE USED AT START OF ASCENT
C
     The user has the ability to change mix, ascent rate, and step size in any
     combination at any depth during the ascent.
C-----
     READ (7,*) Number of Changes
     DO I = 1, Number of Changes
        READ (7,*) Depth_Change(I), Mix Change(I), Rate Change(I),
                  Step_Size_Change(I)
     END DO
     Starting Depth = Depth Change(1)
     Mix_Number = Mix Change(1)
     Rate = Rate Change(1)
     Step Size = Step Size Change(1)
C-----
     CALCULATE THE DEPTH WHERE THE DECOMPRESSION ZONE BEGINS FOR THIS PROFILE
C
     BASED ON THE INITIAL ASCENT PARAMETERS AND WRITE THE DEEPEST POSSIBLE
C
     DECOMPRESSION STOP DEPTH TO THE OUTPUT FILE
C
     Knowing where the decompression zone starts is very important. Below
C
     that depth there is no possibility for bubble formation because there
С
     will be no supersaturation gradients. Deco stops should never start
С
     below the deco zone. The deepest possible stop deco stop depth is
С
     defined as the next "standard" stop depth above the point where the
С
     leading compartment enters the deco zone. Thus, the program will not
С
     base this calculation on step sizes larger than 10 fsw or 3 msw. The
С
     deepest possible stop depth is not used in the program, per se, rather
С
     it is information to tell the diver where to start putting on the brakes
     during ascent. This should be prominently displayed by any deco program.
CALL CALC START OF DECO ZONE (Starting Depth, Rate,
                                                            !subroutine
                               Depth Start of Deco Zone)
     IF (Units Equal Fsw) THEN
         IF (Step Size .LT. 10.0) THEN
            Rounding_Operation1 =
            (Depth Start of Deco Zone/Step Size) - 0.5
            Deepest Possible Stop Depth = ANINT(Rounding Operation1)
            * Step Size
         ELSE
            Rounding Operation1 = (Depth Start of Deco Zone/10.0)
            Deepest_Possible_Stop_Depth = ANINT(Rounding_Operation1)
            * 10.0
        END IF
     END IF
     IF (Units Equal Msw) THEN
         IF (Step Size .LT. 3.0) THEN
            Rounding Operation1 =
            (Depth Start of Deco Zone/Step Size) - 0.5
            Deepest Possible Stop Depth = ANINT (Rounding Operation1)
            * Step Size
         ELSE
            Rounding Operation1 = (Depth Start of Deco Zone/3.0)
            Deepest Possible Stop Depth = ANINT(Rounding Operation1)
            * 3.0
         END IF
     END IF
```

```
WRITE (8,813)
    WRITE (8,813)
    WRITE (8,850)
    WRITE (8,813)
    WRITE (8,857) Depth Start of Deco Zone, Units Word1
    WRITE (8,858) Deepest Possible Stop Depth, Units Word1
    WRITE (8,813)
    WRITE (8,851)
    WRITE (8,852)
    WRITE (8,853) Units Word1, Units Word2, Units Word1
TEMPORARILY ASCEND PROFILE TO THE START OF THE DECOMPRESSION ZONE, SAVE
    VARIABLES AT THIS POINT, AND INITIALIZE VARIABLES FOR CRITICAL VOLUME LOOP
    The iterative process of the VPM Critical Volume Algorithm will operate
С
    only in the decompression zone since it deals with excess gas volume
    released as a result of supersaturation gradients (not possible below the
    decompression zone).
CALL GAS LOADINGS ASCENT DESCENT (Starting Depth, !subroutine
                                 Depth Start of Deco Zone, Rate)
    Run Time Start of Deco Zone = Run Time
    Deco_Phase_Volume_Time = 0.0
    Last_Run_Time = 0.0
    Schedule_Converged = (.FALSE.)
    DO I = 1,16
        Last_Phase_Volume_Time(I) = 0.0
        He_Pressure_Start_of_Deco_Zone(I) = Helium Pressure(I)
        N2 Pressure Start of Deco Zone(I) = Nitrogen Pressure(I)
        Max Actual Gradient(I) = 0.0
    END DO
START OF CRITICAL VOLUME LOOP
    This loop operates between Lines 50 and 100. If the Critical Volume
C
    Algorithm is toggled "off" in the program settings, there will only be
С
    one pass through this loop. Otherwise, there will be two or more passes
С
    through this loop until the deco schedule is "converged" - that is when a
С
    comparison between the phase volume time of the present iteration and the
С
    last iteration is less than or equal to one minute. This implies that
C
    the volume of released gas in the most recent iteration differs from the
C
    "critical" volume limit by an acceptably small amount. The critical
С
    volume limit is set by the Critical Volume Parameter Lambda in the program
    settings (default setting is 7500 fsw-min with adjustability range from
    from 6500 to 8300 fsw-min according to Bruce Wienke).
!loop will run continuously until
   DO 100, WHILE (.TRUE.)
                                      !there is an exit statement
CALCULATE CURRENT DECO CEILING BASED ON ALLOWABLE SUPERSATURATION
    GRADIENTS AND SET FIRST DECO STOP. CHECK TO MAKE SURE THAT SELECTED STEP
С
   SIZE WILL NOT ROUND UP FIRST STOP TO A DEPTH THAT IS BELOW THE DECO ZONE.
CALL CALC DECO CEILING (Deco Ceiling Depth)
                                                        !subroutine
    IF (Deco Ceiling Depth .LE. 0.0) THEN
         Deco Stop Depth = 0.0
         Rounding Operation2 = (Deco Ceiling Depth/Step Size) + 0.5
         Deco Stop Depth = ANINT(Rounding Operation2) * Step Size
    END IF
    IF (Deco Stop Depth .GT. Depth Start of Deco Zone) THEN
        WRITE (*,905)
        WRITE (*,900)
        STOP 'PROGRAM TERMINATED'
```

```
END IF
C
    PERFORM A SEPARATE "PROJECTED ASCENT" OUTSIDE OF THE MAIN PROGRAM TO MAKE
C
    SURE THAT AN INCREASE IN GAS LOADINGS DURING ASCENT TO THE FIRST STOP WILL
    NOT CAUSE A VIOLATION OF THE DECO CEILING. IF SO, ADJUST THE FIRST STOP
C
C
    DEEPER BASED ON STEP SIZE UNTIL A SAFE ASCENT CAN BE MADE.
    Note: this situation is a possibility when ascending from extremely deep
C
С
    dives or due to an unusual gas mix selection.
    CHECK AGAIN TO MAKE SURE THAT ADJUSTED FIRST STOP WILL NOT BE BELOW THE
    DECO ZONE.
CALL PROJECTED ASCENT (Depth Start of Deco Zone, Rate,
                       Deco Stop Depth, Step Size)
    IF (Deco Stop Depth .GT. Depth Start of Deco Zone) THEN
       WRITE (*, 905)
       WRITE (*,900)
        STOP 'PROGRAM TERMINATED'
    END IF
HANDLE THE SPECIAL CASE WHEN NO DECO STOPS ARE REQUIRED - ASCENT CAN BE
    MADE DIRECTLY TO THE SURFACE
    Write ascent data to output file and exit the Critical Volume Loop.
IF (Deco_Stop_Depth .EQ. 0.0) THEN
        DO I = 1,16
           Helium Pressure(I) = He Pressure Start of Ascent(I)
           Nitrogen_Pressure(I) = N2_Pressure Start of Ascent(I)
        END DO
        Run Time = Run Time Start of Ascent
        Segment Number = Segment Number Start of Ascent
        Starting Depth = Depth Change(1)
        Ending Depth = 0.0
        CALL GAS LOADINGS ASCENT DESCENT (Starting Depth,
                                                      !subroutine
                                   Ending Depth, Rate)
        WRITE (8,860) Segment Number, Segment Time, Run Time,
                   Mix Number, Deco Stop Depth, Rate
        EXIT
                              !exit the critical volume loop at Line 100
    END IF
C-----
    ASSIGN VARIABLES FOR ASCENT FROM START OF DECO ZONE TO FIRST STOP. SAVE
    FIRST STOP DEPTH FOR LATER USE WHEN COMPUTING THE FINAL ASCENT PROFILE
Starting Depth = Depth Start of Deco Zone
    First Stop Depth = Deco Stop Depth
DECO STOP LOOP BLOCK WITHIN CRITICAL VOLUME LOOP
С
    This loop computes a decompression schedule to the surface during each
С
    iteration of the critical volume loop. No output is written from this
С
    loop, rather it computes a schedule from which the in-water portion of the
С
    total phase volume time (Deco Phase Volume Time) can be extracted. Also,
С
    the gas loadings computed at the end of this loop are used the subroutine
С
    which computes the out-of-water portion of the total phase volume time
С
    (Surface Phase Volume Time) for that schedule.
C
C
    Note that exit is made from the loop after last ascent is made to a deco
C
    stop depth that is less than or equal to zero. A final deco stop less
    than zero can happen when the user makes an odd step size change during
    ascent - such as specifying a 5 msw step size change at the 3 msw stop!
DO WHILE (.TRUE.)
                                     !loop will run continuously until
                                     !there is an exit statement
```

```
CALL GAS LOADINGS ASCENT DESCENT (Starting_Depth,
                                                                !subroutine
                                        Deco Stop Depth, Rate)
         IF (Deco Stop Depth .LE. 0.0) EXIT
                                                           !exit at Line 60
         IF (Number of Changes .GT. 1) THEN
            DO I = 2, Number of Changes
                IF (Depth_Change(I) .GE. Deco_Stop_Depth) THEN
                    Mix_Number = Mix Change(I)
                    Rate = Rate Change(I)
                    Step Size = Step Size Change(I)
                END IF
            END DO
         END IF
         CALL DECOMPRESSION STOP (Deco Stop Depth, Step Size) !subroutine
         Starting_Depth = Deco_Stop_Depth
         Next Stop = Deco Stop Depth - Step Size
         Deco Stop Depth = Next Stop
         Last Run Time = Run Time
60
     END DO
                                               !end of deco stop loop block
COMPUTE TOTAL PHASE VOLUME TIME AND MAKE CRITICAL VOLUME COMPARISON
     The deco phase volume time is computed from the run time. The surface
C
     phase volume time is computed in a subroutine based on the surfacing gas
С
     loadings from previous deco loop block. Next the total phase volume time
С
     (in-water + surface) for each compartment is compared against the previous
С
     total phase volume time. The schedule is converged when the difference is
С
     less than or equal to 1 minute in any one of the 16 compartments.
C
С
     Note: the "phase volume time" is somewhat of a mathematical concept.
C
     It is the time divided out of a total integration of supersaturation
С
     gradient x time (in-water and surface). This integration is multiplied
С
     by the excess bubble number to represent the amount of free-gas released
     as a result of allowing a certain number of excess bubbles to form.
Deco Phase Volume Time = Run Time - Run Time Start of Deco Zone
     CALL CALC SURFACE PHASE VOLUME TIME
                                                               !subroutine
     DO I = 1,16
         Phase Volume Time(I) = Deco Phase Volume Time +
                              Surface Phase Volume Time(I)
         Critical_Volume_Comparison = ABS(Phase_Volume_Time(I) -
                                   Last_Phase_Volume_Time(I))
         IF (Critical_Volume_Comparison .LE. 1.0) THEN
             Schedule Converged = (.TRUE.)
         END IF
     END DO
CRITICAL VOLUME DECISION TREE BETWEEN LINES 70 AND 99
С
     There are two options here. If the Critical Volume Agorithm setting is
С
     "on" and the schedule is converged, or the Critical Volume Algorithm
С
     setting was "off" in the first place, the program will re-assign variables
С
     to their values at the start of ascent (end of bottom time) and process
С
     a complete decompression schedule once again using all the same ascent
C
     parameters and first stop depth. This decompression schedule will match
С
     the last iteration of the Critical Volume Loop and the program will write
C
     the final deco schedule to the output file.
C
C
     Note: if the Critical Volume Agorithm setting was "off", the final deco
C
     schedule will be based on "Initial Allowable Supersaturation Gradients."
С
     If it was "on", the final schedule will be based on "Adjusted Allowable
С
     Supersaturation Gradients" (gradients that are "relaxed" as a result of
     the Critical Volume Algorithm).
```

```
С
C
    If the Critical Volume Agorithm setting is "on" and the schedule is not
C
    converged, the program will re-assign variables to their values at the
    start of the deco zone and process another trial decompression schedule.
IF ((Schedule Converged) .OR.
                    (Critical Volume Algorithm Off)) THEN
       DO I = 1,16
          Helium Pressure(I) = He Pressure Start of Ascent(I)
          Nitrogen Pressure(I) = N2 Pressure Start of Ascent(I)
       Run Time = Run Time Start of Ascent
       Segment Number = Segment Number Start of Ascent
       Starting Depth = Depth_Change(1)
       Mix Number = Mix Change(1)
       Rate = Rate_Change(1)
       Step_Size = Step_Size_Change(1)
       Deco Stop Depth = First Stop Depth
       Last Run Time = 0.0
DECO STOP LOOP BLOCK FOR FINAL DECOMPRESSION SCHEDULE
DO WHILE (.TRUE.)
                                    !loop will run continuously until
                                    !there is an exit statement
          CALL GAS_LOADINGS_ASCENT_DESCENT (Starting_Depth,
                                                     !subroutine
                                    Deco Stop Depth, Rate)
DURING FINAL DECOMPRESSION SCHEDULE PROCESS, COMPUTE MAXIMUM ACTUAL
    SUPERSATURATION GRADIENT RESULTING IN EACH COMPARTMENT
    If there is a repetitive dive, this will be used later in the VPM
    Repetitive Algorithm to adjust the values for critical radii.
CALL CALC MAX ACTUAL GRADIENT (Deco Stop Depth)
                                                 !subroutine
          WRITE (8,860) Segment Number, Segment Time, Run Time,
                     Mix Number, Deco Stop Depth, Rate
          IF (Deco Stop Depth .LE. 0.0) EXIT
                                                  !exit at Line 80
          IF (Number of Changes .GT. 1) THEN
             DO I = 2, Number of Changes
                 IF (Depth Change (I) .GE. Deco_Stop_Depth) THEN
                    Mix Number = Mix Change(I)
                    Rate = Rate Change(I)
                    Step Size = Step Size Change(I)
                 END IF
             END DO
          END IF
          CALL DECOMPRESSION_STOP (Deco_Stop_Depth, Step_Size) !subroutine
This next bit justs rounds up the stop time at the first stop to be in
    whole increments of the minimum stop time (to make for a nice deco table).
C-----
          IF (Last Run Time .EQ. 0.0) THEN
              Stop Time =
              ANINT((Segment Time/Minimum Deco Stop Time) + 0.5) *
                    Minimum Deco Stop Time
              Stop Time = Run Time - Last Run Time
          END IF
DURING FINAL DECOMPRESSION SCHEDULE, IF MINIMUM STOP TIME PARAMETER IS A
    WHOLE NUMBER (i.e. 1 minute) THEN WRITE DECO SCHEDULE USING INTEGER
C
    NUMBERS (looks nicer). OTHERWISE, USE DECIMAL NUMBERS.
С
    Note: per the request of a noted exploration diver(!), program now allows
```

```
a minimum stop time of less than one minute so that total ascent time can
    be minimized on very long dives. In fact, with step size set at 1 fsw or
C
    0.2 msw and minimum stop time set at 0.1 minute (6 seconds), a near
    continuous decompression schedule can be computed.
IF (AINT(Minimum Deco Stop Time) .EQ.
                                 Minimum Deco Stop Time) THEN
              WRITE (8,862) Segment Number, Segment Time, Run Time,
                      Mix Number, INT (Deco Stop Depth),
                      INT(Stop Time), INT(Run Time)
           ELSE
              WRITE (8,863) Segment Number, Segment Time, Run Time,
                      Mix Number, Deco Stop Depth, Stop Time,
                      Run Time
           END IF
           Starting_Depth = Deco_Stop_Depth
           Next Stop = Deco Stop Depth - Step Size
           Deco Stop Depth = Next Stop
           Last Run Time = Run Time
80
        END DO
                                         !end of deco stop loop block
                                         !for final deco schedule
        EXIT
                                 !exit critical volume loop at Line 100
                                         !final deco schedule written
    ELSE
C-----
    IF SCHEDULE NOT CONVERGED, COMPUTE RELAXED ALLOWABLE SUPERSATURATION
    GRADIENTS WITH VPM CRITICAL VOLUME ALGORITHM AND PROCESS ANOTHER
    ITERATION OF THE CRITICAL VOLUME LOOP
CALL CRITICAL VOLUME (Deco Phase Volume Time)
       Deco Phase Volume Time = 0.0
        Run Time = Run Time Start of Deco Zone
        Starting Depth = Depth Start_of_Deco_Zone
       Mix Number = Mix Change(1)
        Rate = Rate Change(1)
        Step Size = Step Size Change(1)
        DO I = 1,16
           Last Phase_Volume_Time(I) = Phase_Volume_Time(I)
           Helium Pressure(I) = He Pressure Start of Deco Zone(I)
           Nitrogen Pressure(I) = N2 Pressure Start of Deco Zone(I)
        END DO
        CYCLE
                                !Return to start of critical volume loop
                                !(Line 50) to process another iteration
99
    END IF
                                  !end of critical volume decision tree
100
    CONTINUE
                                         !end of critical volume loop
PROCESSING OF DIVE COMPLETE. READ INPUT FILE TO DETERMINE IF THERE IS A
    REPETITIVE DIVE. IF NONE, THEN EXIT REPETITIVE LOOP.
READ (7,*) Repetitive Dive Flag
    IF (Repetitive Dive Flag .EQ. 0) THEN
        EXIT
                                           !exit repetitive dive loop
                                          !at Line 330
IF THERE IS A REPETITIVE DIVE, COMPUTE GAS LOADINGS (OFF-GASSING) DURING
    SURFACE INTERVAL TIME. ADJUST CRITICAL RADII USING VPM REPETITIVE
C
    ALGORITHM. RE-INITIALIZE SELECTED VARIABLES AND RETURN TO START OF
    REPETITIVE LOOP AT LINE 30.
```

```
ELSE IF (Repetitive Dive Flag .EQ. 1) THEN
        READ (7,*) Surface Interval Time
        CALL GAS LOADINGS SURFACE INTERVAL (Surface Interval Time) !subroutine
        CALL VPM REPETITIVE ALGORITHM (Surface Interval Time)
                                                    !subroutine
        DO I = 1,16
           Max Crushing Pressure He(I) = 0.0
           Max Crushing Pressure N2(I) = 0.0
           Max Actual Gradient(I) = 0.0
        END DO
        Run Time = 0.0
        Segment Number = 0
        WRITE (8,880)
        WRITE (8,890)
        WRITE (8,813)
                !Return to start of repetitive loop to process another dive
WRITE ERROR MESSAGE AND TERMINATE PROGRAM IF THERE IS AN ERROR IN THE
    INPUT FILE FOR THE REPETITIVE DIVE FLAG
CALL SYSTEMQQ (OS Command)
        WRITE (*,908)
        WRITE (*,900)
        STOP 'PROGRAM TERMINATED'
    END IF
330 CONTINUE
                                               !End of repetitive loop
FINAL WRITES TO OUTPUT AND CLOSE PROGRAM FILES
WRITE (*,813)
    WRITE (*,871)
    WRITE (*,872)
    WRITE (*,813)
    WRITE (8,880)
    CLOSE (UNIT = 7, STATUS = 'KEEP')
    CLOSE (UNIT = 8, STATUS = 'KEEP')
    CLOSE (UNIT = 10, STATUS = 'KEEP')
FORMAT STATEMENTS - PROGRAM INPUT/OUTPUT
FORMAT ('OUNITS = FEET OF SEAWATER (FSW)')
    FORMAT ('OUNITS = METERS OF SEAWATER (MSW)')
    FORMAT ('OALTITUDE = ',1X,F7.1,4X,'BAROMETRIC PRESSURE = ',
802
    *F6.3)
805
    FORMAT (A70)
    FORMAT ('-E-&a10L-&180F-&18D-(s0p16.67h8.5')
810
    FORMAT (26X, 'DECOMPRESSION CALCULATION PROGRAM')
811
812
    FORMAT (24X, 'Developed in FORTRAN by Erik C. Baker')
814
    FORMAT ('Program Run:',4X,I2.2,'-',I2.2,'-',I4,1X,'at',1X,I2.2,
           ':',I2.2,1X,A1,'m',23X,'Model: VPM 2001')
815
    FORMAT ('Description:',4X,A70)
    FORMAT ('')
    FORMAT ('Gasmix Summary:',24X,'FO2',4X,'FHe',4X,'FN2')
820
    FORMAT (26X, 'Gasmix #', I2, 2X, F5.3, 2X, F5.3, 2X, F5.3)
821
830
    FORMAT (36X, 'DIVE PROFILE')
    FORMAT ('Seg-',2X,'Segm.',2X,'Run',3X,'|',1X,'Gasmix',1X,'|',1X,
831
          'Ascent', 4X, 'From', 5X, 'To', 6X, 'Rate', 4X, '|', 1X, 'Constant')
    FORMAT ('ment', 2X, 'Time', 3X, 'Time', 2X, '|', 2X, 'Used', 2X, '|', 3X,
832
           'or',5X,'Depth',3X,'Depth',4X,'+Dn/-Up',2X,'|',2X,'Depth')
    FORMAT (2X, '#', 3X, '(min)', 2X, '(min)', 1X, '|', 4X, '#', 3X, '|', 1X,
833
```

```
'Descent',2X,'(',A4,')',2X,'(',A4,')',2X,'(',A7,')',1X,
            '|',2X,'(',A4,')')
834
    FORMAT ('----',1X,'----',2X,'----',1X,'|',1X,'-----',1X,'|',
            1X,'----',2X,'-----',2X,'-----',1X,
            '|',1X,'----')
840
    FORMAT (I3,3X,F5.1,1X,F6.1,1X,'|',3X,I2,3X,'|',1X,A7,F7.0,
               1X, F7.0, 3X, F7.1, 3X, '|')
    FORMAT (I3,3X,F5.1,1X,F6.1,1X,'|',3X,I2,3X,'|',36X,'|',F7.0)
845
     FORMAT (31X, 'DECOMPRESSION PROFILE')
850
     FORMAT ('Seq-',2X,'Seqm.',2X,'Run',3X,'|',1X,'Gasmix',1X,'|',1X,
851
            'Ascent', 3X, 'Ascent', 3X, 'Col', 3X, '|', 2X, 'DECO', 3X, 'STOP',
            3X,'RUN')
     FORMAT ('ment', 2X, 'Time', 3X, 'Time', 2X, '|', 2X, 'Used', 2X, '|', 3X,
852
            'To',6X,'Rate',4X,'Not',3X,'|',2X,'STOP',3X,'TIME',3X,
            'TIME')
     FORMAT (2X, '#', 3X, '(min)', 2X, '(min)', 1X, '|', 4X, '#', 3X, '|', 1X,
853
            '(',A4,')',1X,'(',A7,')',2X,'Used',2X,'|',1X,'(',A4,')',
            2X,'(min)',2X,'(min)')
     FORMAT ('----',1X,'----',2X,'----',1X,'|',1X,'----',1X,'|',
854
            1X,'----',1X,'-----',1X,'----',1X,'|',1X,
           '----',2X,'----',2X,'----')
857
    FORMAT (10X, 'Leading compartment enters the decompression zone',
            1X, 'at', F7.1, 1X, A4)
858
     FORMAT (17X, 'Deepest possible decompression stop is', F7.1, 1X, A4)
860
    FORMAT (I3,3X,F5.1,1X,F6.1,1X,'|',3X,I2,3X,'|',2X,F4.0,3X,F6.1,
            10X,'|')
    FORMAT (I3,3X,F5.1,1X,F6.1,1X,'|',3X,I2,3X,'|',25X,'|',2X,I4,3X,
862
            I4,2X,I5)
863
    FORMAT (I3,3X,F5.1,1X,F6.1,1X,'|',3X,I2,3X,'|',25X,'|',2X,F5.0,1X,
           F6.1,1X,F7.1)
    FORMAT (' PROGRAM CALCULATIONS COMPLETE')
871
    FORMAT ('00utput data is located in the file VPMDECO.OUT')
872
880
    FORMAT ('')
    FORMAT ('REPETITIVE DIVE:')
890
FORMAT STATEMENTS - ERROR MESSAGES
FORMAT ('')
900
    FORMAT ('OERROR! UNITS MUST BE FSW OR MSW')
901
    FORMAT ('OERROR! ALTITUDE DIVE ALGORITHM MUST BE ON OR OFF')
902
    FORMAT ('OERROR! RADIUS MUST BE BETWEEN 0.2 AND 1.35 MICRONS')
903
    FORMAT ('OERROR! CRITICAL VOLUME ALGORITHM MUST BE ON OR OFF')
904
    FORMAT ('OERROR! STEP SIZE IS TOO LARGE TO DECOMPRESS')
905
906
    FORMAT ('OERROR IN INPUT FILE (GASMIX DATA)')
    FORMAT ('OERROR IN INPUT FILE (PROFILE CODE)')
    FORMAT ('OERROR IN INPUT FILE (REPETITIVE DIVE CODE)')
END OF MAIN PROGRAM
C-----
     END
NOTE ABOUT PRESSURE UNITS USED IN CALCULATIONS:
     It is the convention in decompression calculations to compute all gas
С
     loadings, absolute pressures, partial pressures, etc., in the units of
C
     depth pressure that you are diving - either feet of seawater (fsw) or
C
    meters of seawater (msw). This program follows that convention with the
C
    the exception that all VPM calculations are performed in SI units (by
C
    necessity). Accordingly, there are several conversions back and forth
    between the diving pressure units and the SI units.
C-----
```

```
FUNCTION SUBPROGRAM FOR GAS LOADING CALCULATIONS - ASCENT AND DESCENT
FUNCTION SCHREINER EQUATION (Initial Inspired Gas Pressure,
   *Rate Change Insp Gas Pressure, Interval Time, Gas Time Constant,
   *Initial Gas Pressure)
C-----
   ARGUMENTS
REAL Initial Inspired Gas Pressure
   REAL Rate Change Insp Gas Pressure
   REAL Interval Time, Gas Time Constant
                                             !input
   REAL Initial Gas Pressure
                                             !input
   REAL SCHREINER EQUATION
Note: The Schreiner equation is applied when calculating the uptake or
   elimination of compartment gases during linear ascents or descents at a
   constant rate. For ascents, a negative number for rate must be used.
C-----
   SCHREINER EQUATION =
   *Initial Inspired Gas Pressure + Rate Change Insp Gas Pressure*
   *(Interval_Time - 1.0/Gas_Time_Constant) -
   *(Initial_Inspired_Gas_Pressure - Initial_Gas_Pressure -
   *Rate_Change_Insp_Gas_Pressure/Gas_Time_Constant) *
   *EXP (-Gas Time Constant*Interval Time)
   END
FUNCTION SUBPROGRAM FOR GAS LOADING CALCULATIONS - CONSTANT DEPTH
FUNCTION HALDANE EQUATION (Initial Gas Pressure,
   *Inspired Gas Pressure, Gas Time Constant, Interval Time)
ARGUMENTS
REAL Initial Gas Pressure, Inspired Gas Pressure
   REAL Gas Time Constant, Interval Time
                                             !input
   REAL HALDANE EQUATION
                                            !output
Note: The Haldane equation is applied when calculating the uptake or
   elimination of compartment gases during intervals at constant depth (the
   outside ambient pressure does not change).
HALDANE_EQUATION = Initial_Gas_Pressure +
   *(Inspired_Gas_Pressure - Initial_Gas_Pressure)*
   *(1.0 - EXP(-Gas_Time_Constant * Interval_Time))
   RETURN
   END
SUBROUTINE GAS LOADINGS ASCENT DESCENT
   Purpose: This subprogram applies the Schreiner equation to update the
   gas loadings (partial pressures of helium and nitrogen) in the half-time
   compartments due to a linear ascent or descent segment at a constant rate.
SUBROUTINE GAS LOADINGS ASCENT DESCENT (Starting Depth,
                            Ending Depth, Rate)
   IMPLICIT NONE
ARGUMENTS
```

```
REAL Starting Depth, Ending Depth, Rate
                                                   !input
C LOCAL VARIABLES
INTEGER I
                                              !loop counter
    INTEGER Last Segment Number
    REAL Initial Inspired He Pressure
    REAL Initial Inspired N2 Pressure
    REAL Last Run Time
   REAL Helium Rate, Nitrogen Rate, Starting_Ambient_Pressure
   REAL SCHREINER EQUATION
                                         !function subprogram
GLOBAL CONSTANTS IN NAMED COMMON BLOCKS
REAL Water Vapor Pressure
   COMMON /Block_8/ Water_Vapor_Pressure
GLOBAL VARIABLES IN NAMED COMMON BLOCKS
INTEGER Segment Number
                                               !both input
    REAL Run_Time, Segment_Time
                                               !and output
    COMMON /Block 2/ Run Time, Segment Number, Segment Time
    REAL Ending Ambient Pressure
                                                  !output
    COMMON /Block 4/ Ending Ambient Pressure
    INTEGER Mix Number
    COMMON /Block 9/ Mix Number
    REAL Barometric Pressure
   COMMON /Block 18/ Barometric Pressure
GLOBAL ARRAYS IN NAMED COMMON BLOCKS
REAL Helium Time Constant (16)
    COMMON /Block 1A/ Helium Time Constant
    REAL Nitrogen Time Constant (16)
    COMMON /Block 1B/ Nitrogen Time Constant
    REAL Helium_Pressure(16), Nitrogen_Pressure(16)
                                               !both input
   COMMON /Block_3/ Helium_Pressure, Nitrogen_Pressure
                                               !and output
    REAL Fraction Helium(10), Fraction Nitrogen(10)
    COMMON /Block 5/ Fraction Helium, Fraction Nitrogen
   REAL Initial Helium Pressure(16), Initial Nitrogen Pressure(16) !output
   COMMON /Block_23/ Initial_Helium_Pressure,
     Initial_Nitrogen_Pressure
CALCULATIONS
Segment Time = (Ending Depth - Starting Depth)/Rate
    Last Run Time = Run Time
    Run Time = Last Run Time + Segment Time
    Last Segment Number = Segment Number
    Segment Number = Last Segment Number + 1
    Ending Ambient Pressure = Ending Depth + Barometric Pressure
    Starting Ambient Pressure = Starting Depth + Barometric Pressure
   Initial_Inspired_He_Pressure = (Starting_Ambient_Pressure -
              Water Vapor Pressure) *Fraction Helium (Mix Number)
    Initial Inspired N2 Pressure = (Starting Ambient Pressure -
```

```
Water Vapor Pressure) *Fraction Nitrogen (Mix Number)
     Helium Rate = Rate*Fraction Helium(Mix Number)
     Nitrogen Rate = Rate*Fraction Nitrogen(Mix Number)
     DO I = 1,16
        Initial Helium Pressure(I) = Helium Pressure(I)
        Initial Nitrogen Pressure(I) = Nitrogen Pressure(I)
        Helium Pressure(I) = SCHREINER EQUATION
            (Initial Inspired He Pressure, Helium Rate,
            Segment Time, Helium Time Constant(I),
            Initial Helium Pressure(I))
        Nitrogen Pressure(I) = SCHREINER EQUATION
            (Initial Inspired N2 Pressure, Nitrogen Rate,
            Segment Time, Nitrogen Time Constant(I),
            Initial Nitrogen Pressure(I))
     END DO
END OF SUBROUTINE
RETURN
     END
SUBROUTINE CALC CRUSHING PRESSURE
     Purpose: Compute the effective "crushing pressure" in each compartment as
С
     a result of descent segment(s). The crushing pressure is the gradient
С
     (difference in pressure) between the outside ambient pressure and the
С
С
     gas tension inside a VPM nucleus (bubble seed). This gradient acts to
С
     reduce (shrink) the radius smaller than its initial value at the surface.
С
     This phenomenon has important ramifications because the smaller the radius
С
     of a VPM nucleus, the greater the allowable supersaturation gradient upon
С
     ascent. Gas loading (uptake) during descent, especially in the fast
С
     compartments, will reduce the magnitude of the crushing pressure. The
C
     crushing pressure is not cumulative over a multi-level descent. It will
C
     be the maximum value obtained in any one discrete segment of the overall
C
     descent. Thus, the program must compute and store the maximum crushing
C
     pressure for each compartment that was obtained across all segments of
С
     the descent profile.
С
С
     The calculation of crushing pressure will be different depending on
С
     whether or not the gradient is in the VPM permeable range (gas can diffuse
С
     across skin of VPM nucleus) or the VPM impermeable range (molecules in
С
     skin of nucleus are squeezed together so tight that gas can no longer
C
     diffuse in or out of nucleus; the gas becomes trapped and further resists
C
     the crushing pressure). The solution for crushing pressure in the VPM
С
     permeable range is a simple linear equation. In the VPM impermeable
C
     range, a cubic equation must be solved using a numerical method.
С
С
     Separate crushing pressures are tracked for helium and nitrogen because
С
     they can have different critical radii. The crushing pressures will be
C
     the same for helium and nitrogen in the permeable range of the model, but
С
     they will start to diverge in the impermeable range. This is due to
С
     the differences between starting radius, radius at the onset of
     impermeability, and radial compression in the impermeable range.
SUBROUTINE CALC CRUSHING PRESSURE (Starting Depth, Ending Depth,
     IMPLICIT NONE
REAL Starting Depth, Ending Depth, Rate
```

```
LOCAL VARIABLES
INTEGER I
                                                  !loop counter
    REAL Starting Ambient Pressure, Ending Ambient Pressure
    REAL Starting Gas Tension, Ending Gas Tension
    REAL Crushing Pressure He, Crushing Pressure N2
    REAL Gradient Onset of Imperm, Gradient Onset of Imperm Pa
    REAL Ending Ambient Pressure Pa, Amb Press Onset of Imperm Pa
    REAL Gas Tension Onset of Imperm Pa
    REAL Crushing Pressure Pascals He, Crushing Pressure Pascals N2
    REAL Starting Gradient, Ending Gradient
    REAL A He, B He, C He, Ending Radius He, High Bound He
    REAL Low Bound He
    REAL A_N2, B_N2, C_N2, Ending Radius N2, High Bound N2
    REAL Low Bound N2
    REAL Radius_Onset_of_Imperm_He, Radius_Onset_of_Imperm_N2
GLOBAL CONSTANTS IN NAMED COMMON BLOCKS
REAL Gradient Onset of Imperm Atm
    COMMON /Block 14/ Gradient Onset of Imperm Atm
    REAL Constant_Pressure_Other_Gases
    COMMON /Block 17/ Constant Pressure Other Gases
    REAL Surface Tension Gamma, Skin Compression GammaC
    COMMON /Block 19/ Surface Tension Gamma, Skin Compression GammaC
GLOBAL VARIABLES IN NAMED COMMON BLOCKS
REAL Units Factor
    COMMON /Block_16/ Units_Factor
    REAL Barometric Pressure
    COMMON /Block 18/ Barometric Pressure
GLOBAL ARRAYS IN NAMED COMMON BLOCKS
REAL Helium Pressure (16), Nitrogen Pressure (16)
                                                       !input
    COMMON /Block 3/ Helium Pressure, Nitrogen Pressure
    REAL Adjusted Critical Radius He(16)
                                                       !input
    REAL Adjusted_Critical_Radius_N2(16)
COMMON /Block_7/ Adjusted_Critical_Radius_He,
            Adjusted Critical Radius N2
    REAL Max Crushing Pressure He(16), Max Crushing Pressure N2(16) !output
    COMMON /Block_10/ Max_Crushing_Pressure_He,
                 Max Crushing Pressure N2
    REAL Amb Pressure Onset of Imperm(16)
                                                       !input
    REAL Gas Tension Onset of Imperm (16)
    COMMON /Block 13/ Amb Pressure Onset of Imperm,
             Gas Tension Onset of Imperm
    REAL Initial Helium Pressure (16), Initial Nitrogen Pressure (16)
    COMMON /Block 23/ Initial Helium Pressure,
                Initial Nitrogen Pressure
C
    First, convert the Gradient for Onset of Impermeability from units of
С
    atmospheres to diving pressure units (either fsw or msw) and to Pascals
```

```
(SI units). The reason that the Gradient for Onset of Impermeability is
    given in the program settings in units of atmospheres is because that is
C
    how it was reported in the original research papers by Yount and
    colleauges.
Gradient Onset of Imperm = Gradient Onset of Imperm Atm !convert to
                        * Units Factor
                                                 !diving units
                                                  !convert to
    Gradient Onset of Imperm Pa = Gradient Onset of Imperm Atm
                          * 101325.0
Assign values of starting and ending ambient pressures for descent segment
Starting Ambient Pressure = Starting Depth + Barometric Pressure
    Ending Ambient Pressure = Ending Depth + Barometric Pressure
MAIN LOOP WITH NESTED DECISION TREE
C
    For each compartment, the program computes the starting and ending
С
    gas tensions and gradients. The VPM is different than some dissolved gas
    algorithms, Buhlmann for example, in that it considers the pressure due to
    oxygen, carbon dioxide, and water vapor in each compartment in addition to
    the inert gases helium and nitrogen. These "other gases" are included in
    the calculation of gas tensions and gradients.
DO I = 1,16
       Starting_Gas_Tension = Initial_Helium_Pressure(I) +
         Initial Nitrogen Pressure(I) + Constant Pressure Other Gases
       Starting Gradient = Starting Ambient Pressure -
                      Starting Gas Tension
       Ending Gas Tension = Helium Pressure(I) + Nitrogen Pressure(I)
                       + Constant Pressure Other Gases
       Ending Gradient = Ending Ambient Pressure - Ending Gas Tension
Compute radius at onset of impermeability for helium and nitrogen
   critical radii
Radius Onset of Imperm He = 1.0/(Gradient Onset of Imperm Pa/
          (2.0*(Skin Compression GammaC-Surface Tension Gamma)) +
          1.0/Adjusted Critical Radius He(I))
       Radius Onset of Imperm N2 = 1.0/(Gradient Onset of Imperm Pa/
          (2.0*(Skin Compression GammaC-Surface Tension Gamma)) +
          1.0/Adjusted_Critical_Radius_N2(I))
FIRST BRANCH OF DECISION TREE - PERMEABLE RANGE
    Crushing pressures will be the same for helium and nitrogen
C-----
       IF (Ending Gradient .LE. Gradient Onset of Imperm) THEN
          Crushing Pressure He = Ending Ambient Pressure -
                           Ending Gas Tension
          Crushing Pressure N2 = Ending Ambient Pressure -
                           Ending Gas Tension
SECOND BRANCH OF DECISION TREE - IMPERMEABLE RANGE
C
    Both the ambient pressure and the gas tension at the onset of
С
    impermeability must be computed in order to properly solve for the ending
    radius and resultant crushing pressure. The first decision block
С
    addresses the special case when the starting gradient just happens to be
```

```
equal to the gradient for onset of impermeability (not very likely!).
IF (Ending Gradient .GT. Gradient Onset of Imperm) THEN
            IF (Starting Gradient .EQ. Gradient Onset of Imperm) THEN
               Amb_Pressure_Onset_of_Imperm(I) =
                                   Starting Ambient Pressure
               Gas Tension Onset of Imperm(I) = Starting Gas Tension
            END IF
In most cases, a subroutine will be called to find these values using a
    numerical method.
IF (Starting Gradient .LT. Gradient Onset of Imperm) THEN
               CALL ONSET_OF_IMPERMEABILITY
                                                            !subroutine
                            (Starting Ambient Pressure,
                            Ending_Ambient_Pressure, Rate, I)
            END IF
Next, using the values for ambient pressure and gas tension at the onset
     of impermeability, the equations are set up to process the calculations through the radius root finder subroutine. This subprogram will find the
С
C
С
     root (solution) to the cubic equation using a numerical method. In order
С
     to do this efficiently, the equations are placed in the form
     Ar^3 - Br^2 - C = 0, where r is the ending radius after impermeable
С
С
     compression. The coefficients A, B, and C for helium and nitrogen are
    computed and passed to the subroutine as arguments. The high and low
С
С
     bounds to be used by the numerical method of the subroutine are also
С
     computed (see separate page posted on Deco List ftp site entitled
С
     "VPM: Solving for radius in the impermeable regime"). The subprogram
С
     will return the value of the ending radius and then the crushing
    pressures for helium and nitrogen can be calculated.
Ending Ambient Pressure Pa =
                (Ending Ambient Pressure/Units Factor) * 101325.0
            Amb Press Onset of Imperm Pa =
                (Amb Pressure Onset of Imperm(I)/Units Factor)
                * 101325.0
            Gas Tension Onset of Imperm Pa =
                (Gas Tension Onset of Imperm(I)/Units Factor)
            B He = 2.0*(Skin Compression GammaC-Surface Tension Gamma)
            A_He = Ending_Ambient_Pressure_Pa -
               Amb_Press_Onset_of_Imperm_Pa +
               Gas_Tension_Onset_of_Imperm_Pa +
                (2.0*(Skin Compression GammaC-Surface Tension Gamma))
               /Radius Onset of Imperm He
            C He = Gas Tension Onset of Imperm Pa *
               Radius Onset of Imperm He**3
            High Bound He = Radius Onset of Imperm He
            Low Bound He = B He/A He
            CALL RADIUS ROOT FINDER (A He, B He, C He,
                                                            !subroutine
                  Low Bound He, High Bound He, Ending Radius He)
            Crushing Pressure Pascals He =
               Gradient Onset of Imperm Pa +
```

```
Ending Ambient Pressure Pa -
             Amb Press Onset of Imperm Pa +
             Gas_Tension_Onset_of_Imperm_Pa *
              (1.0-Radius Onset of Imperm He**3/Ending Radius He**3)
          Crushing Pressure He =
              (Crushing Pressure Pascals He/101325.0) * Units Factor
          B N2 = 2.0*(Skin Compression GammaC-Surface Tension Gamma)
          A N2 = Ending Ambient Pressure Pa -
             Amb Press Onset of Imperm Pa +
             Gas Tension Onset of Imperm Pa +
              (2.0*(Skin Compression_GammaC-Surface_Tension_Gamma))
             /Radius Onset of Imperm N2
          C N2 = Gas Tension Onset of Imperm Pa *
             Radius_Onset_of_Imperm_N2**3
          High Bound N2 = Radius Onset of Imperm N2
          Low Bound \overline{N}2 = B N2/A \overline{N}2
          CALL RADIUS ROOT FINDER (A N2, B N2, C N2,
                                                    !subroutine
                Low Bound N2, High Bound N2, Ending Radius N2)
          Crushing_Pressure_Pascals_N2 =
             Gradient_Onset_of_Imperm_Pa +
             Ending Ambient Pressure Pa -
             Amb Press Onset of Imperm Pa +
             Gas Tension Onset of Imperm Pa *
             (1.0-Radius Onset of Imperm N2**3/Ending Radius N2**3)
          Crushing Pressure N2 =
              (Crushing Pressure Pascals N2/101325.0) * Units Factor
UPDATE VALUES OF MAX CRUSHING PRESSURE IN GLOBAL ARRAYS
Max Crushing Pressure He(I) = MAX(Max_Crushing_Pressure_He(I),
                                     Crushing Pressure He)
       Max Crushing Pressure N2(I) = MAX(Max Crushing Pressure N2(I),
                                     Crushing Pressure N2)
    END DO
END OF SUBROUTINE
RETURN
    END
SUBROUTINE ONSET OF IMPERMEABILITY
    Purpose: This subroutine uses the Bisection Method to find the ambient
    pressure and gas tension at the onset of impermeability for a given
    compartment. Source: "Numerical Recipes in Fortran 77",
   Cambridge University Press, 1992.
SUBROUTINE ONSET OF IMPERMEABILITY (Starting Ambient Pressure,
                          Ending Ambient Pressure, Rate, I)
    IMPLICIT NONE
ARGUMENTS
```

```
INTEGER I
                             !input - array subscript for compartment
    REAL Starting_Ambient_Pressure, Ending_Ambient_Pressure, Rate
LOCAL VARIABLES
INTEGER J
                                                !loop counter
    REAL Initial Inspired He Pressure
    REAL Initial Inspired N2 Pressure, Time
    REAL Helium Rate, Nitrogen Rate
    REAL Low Bound, High Bound, High Bound Helium Pressure
    REAL High Bound Nitrogen Pressure, Mid Range Helium Pressure
    REAL Mid Range Nitrogen Pressure, Last Diff Change
    REAL Function at High Bound, Function_at_Low_Bound
    REAL Mid_Range_Time, Function_at_Mid_Range, Differential_Change
    REAL Mid Range Ambient Pressure, Gas Tension at Mid Range
    REAL Gradient Onset of Imperm
    REAL Starting Gas Tension, Ending Gas Tension
    REAL SCHREINER EQUATION
                                           !function subprogram
GLOBAL CONSTANTS IN NAMED COMMON BLOCKS
REAL Water_Vapor_Pressure
    COMMON /Block_8/ Water_Vapor_Pressure
    REAL Gradient Onset of Imperm Atm
    COMMON /Block_14/ Gradient_Onset of Imperm Atm
    REAL Constant Pressure Other Gases
    COMMON /Block 17/ Constant Pressure Other Gases
GLOBAL VARIABLES IN NAMED COMMON BLOCKS
INTEGER Mix Number
    COMMON /Block 9/ Mix Number
    REAL Units Factor
    COMMON /Block 16/ Units Factor
GLOBAL ARRAYS IN NAMED COMMON BLOCKS
REAL Helium Time Constant (16)
    COMMON /Block_1A/ Helium_Time_Constant
    REAL Nitrogen_Time_Constant(16)
    COMMON /Block_1B/ Nitrogen_Time_Constant
    REAL Fraction Helium(10), Fraction Nitrogen(10)
    COMMON /Block 5/ Fraction Helium, Fraction Nitrogen
    REAL Amb Pressure Onset of Imperm(16)
                                                     !output
    REAL Gas Tension Onset of Imperm (16)
    COMMON /Block 13/ Amb Pressure Onset of Imperm,
             Gas Tension Onset of Imperm
    REAL Initial Helium Pressure (16), Initial Nitrogen Pressure (16)
    COMMON /Block 23/ Initial Helium Pressure,
                Initial Nitrogen Pressure
C
С
    First convert the Gradient for Onset of Impermeability to the diving
    pressure units that are being used
```

```
Gradient Onset of Imperm = Gradient Onset of Imperm Atm
              * Units_Factor
ESTABLISH THE BOUNDS FOR THE ROOT SEARCH USING THE BISECTION METHOD
C
    In this case, we are solving for time - the time when the ambient pressure
    minus the gas tension will be equal to the Gradient for Onset of
С
С
    Impermeabliity. The low bound for time is set at zero and the high
C
    bound is set at the elapsed time (segment time) it took to go from the
С
    starting ambient pressure to the ending ambient pressure. The desired
C
     ambient pressure and gas tension at the onset of impermeability will
    be found somewhere between these endpoints. The algorithm checks to
    make sure that the solution lies in between these bounds by first
    computing the low bound and high bound function values.
Initial_Inspired_He_Pressure = (Starting_Ambient_Pressure -
                 Water Vapor Pressure) *Fraction Helium (Mix Number)
    Initial Inspired N2 Pressure = (Starting Ambient Pressure -
                Water Vapor Pressure) *Fraction Nitrogen (Mix Number)
     Helium Rate = Rate*Fraction Helium(Mix Number)
     Nitrogen Rate = Rate*Fraction Nitrogen(Mix Number)
    Low Bound = 0.0
    High Bound = (Ending Ambient Pressure - Starting Ambient Pressure)
                /Rate
    Starting Gas Tension = Initial Helium Pressure(I) +
          Initial Nitrogen Pressure(I) + Constant Pressure Other Gases
    Function at Low Bound = Starting Ambient Pressure -
                    Starting Gas Tension - Gradient Onset of Imperm
    High Bound Helium Pressure = SCHREINER EQUATION
        (Initial Inspired He Pressure, Helium Rate,
        High Bound, Helium Time Constant (I),
        Initial Helium Pressure(I))
    High Bound Nitrogen Pressure = SCHREINER EQUATION
        High Bound, Nitrogen Time Constant (I),
        Initial Nitrogen Pressure(I))
    Ending_Gas_Tension = High_Bound_Helium_Pressure +
          High Bound Nitrogen Pressure + Constant Pressure Other Gases
    Function_at_High_Bound = Ending_Ambient_Pressure -
                      Ending Gas Tension - Gradient Onset of Imperm
     IF ((Function at High Bound*Function at Low Bound) .GE. 0.0) THEN
        PRINT *, 'ERROR! ROOT IS NOT WITHIN BRACKETS'
        PAUSE
    END IF
APPLY THE BISECTION METHOD IN SEVERAL ITERATIONS UNTIL A SOLUTION WITH
    THE DESIRED ACCURACY IS FOUND
    Note: the program allows for up to 100 iterations. Normally an exit will
    be made from the loop well before that number. If, for some reason, the
    program exceeds 100 iterations, there will be a pause to alert the user.
IF (Function at Low Bound .LT. 0.0) THEN
        Time = Low Bound
        Differential Change = High Bound - Low Bound
```

ELSE

```
Time = High Bound
       Differential Change = Low Bound - High Bound
    END IF
    DO J = 1, 100
       Last Diff Change = Differential Change
       Differential Change = Last Diff Change*0.5
       Mid Range Time = Time + Differential Change
       Mid Range Ambient Pressure = (Starting Ambient Pressure +
                               Rate*Mid Range Time)
       Mid Range Helium Pressure = SCHREINER EQUATION
           (Initial Inspired He Pressure, Helium Rate,
          Mid Range Time, Helium Time_Constant(I),
           Initial_Helium_Pressure(I))
       Mid_Range_Nitrogen_Pressure = SCHREINER_EQUATION
           (Initial Inspired N2 Pressure, Nitrogen Rate,
           Mid Range Time, Nitrogen Time Constant (I),
           Initial Nitrogen Pressure(I))
       Gas Tension at Mid Range = Mid Range Helium Pressure +
          Mid Range Nitrogen Pressure + Constant Pressure Other Gases
       Function at Mid Range = Mid Range Ambient Pressure -
           Gas Tension at Mid Range - Gradient Onset of Imperm
       IF (Function at Mid Range .LE. 0.0) Time = Mid Range Time
       IF ((ABS(Differential Change) .LT. 1.0E-3) .OR.
           (Function at Mid Range .EQ. 0.0)) GOTO 100
    PRINT *, 'ERROR! ROOT SEARCH EXCEEDED MAXIMUM ITERATIONS'
When a solution with the desired accuracy is found, the program jumps out
    of the loop to Line 100 and assigns the solution values for ambient
    pressure and gas tension at the onset of impermeability.
100 Amb Pressure Onset of Imperm(I) = Mid Range Ambient Pressure
    Gas_Tension_Onset_of_Imperm(I) = Gas_Tension_at_Mid_Range
END OF SUBROUTINE
RETURN
    END
SUBROUTINE RADIUS ROOT FINDER
C
    Purpose: This subroutine is a "fail-safe" routine that combines the
С
    Bisection Method and the Newton-Raphson Method to find the desired root.
    This hybrid algorithm takes a bisection step whenever Newton-Raphson would
    take the solution out of bounds, or whenever Newton-Raphson is not
    converging fast enough. Source: "Numerical Recipes in Fortran 77",
    Cambridge University Press, 1992.
SUBROUTINE RADIUS ROOT FINDER (A,B,C, Low Bound, High Bound,
                            Ending Radius)
    IMPLICIT NONE
ARGUMENTS
```

```
REAL A, B, C, Low Bound, High Bound
    REAL Ending Radius
                                                        !output
LOCAL VARIABLES
!loop counter
    REAL Function, Derivative of Function, Differential Change
    REAL Last Diff Change, Last Ending Radius
    REAL Radius at Low Bound, Radius at High Bound
    REAL Function at Low Bound, Function at High Bound
BEGIN CALCULATIONS BY MAKING SURE THAT THE ROOT LIES WITHIN BOUNDS
    In this case we are solving for radius in a cubic equation of the form,
C
    Ar^3 - Br^2 - C = 0. The coefficients A, B, and C were passed to this
    subroutine as arguments.
Function at Low Bound =
       Low Bound* (Low Bound* (A*Low Bound - B)) - C
    Function at High Bound =
       High Bound* (High Bound* (A*High Bound - B)) - C
    IF ((Function_at_Low_Bound .GT. 0.0).AND.
       (Function_at_High Bound .GT. 0.0)) THEN
       PRINT *, 'ERROR! ROOT IS NOT WITHIN BRACKETS'
       PAUSE
    END IF
Next the algorithm checks for special conditions and then prepares for
    the first bisection.
IF ((Function at Low Bound .LT. 0.0).AND.
       (Function at High Bound .LT. 0.0)) THEN
       PRINT *, 'ERROR! ROOT IS NOT WITHIN BRACKETS'
       PAUSE
    END IF
    IF (Function at Low Bound .EQ. 0.0) THEN
       Ending Radius = Low Bound
       RETURN
    ELSE IF (Function at High Bound .EQ. 0.0) THEN
       Ending Radius = High Bound
    ELSE IF (Function_at_Low_Bound .LT. 0.0) THEN
       Radius_at_Low_Bound = Low_Bound
       Radius at High Bound = High Bound
    ELSE
       Radius at High Bound = Low Bound
       Radius at Low Bound = High Bound
    END IF
    Ending Radius = 0.5*(Low Bound + High Bound)
    Last Diff Change = ABS (High Bound-Low Bound)
    Differential Change = Last Diff Change
At this point, the Newton-Raphson Method is applied which uses a function
    and its first derivative to rapidly converge upon a solution.
    Note: the program allows for up to 100 iterations. Normally an exit will
C
    be made from the loop well before that number. If, for some reason, the
C
C
    program exceeds 100 iterations, there will be a pause to alert the user.
    When a solution with the desired accuracy is found, exit is made from the
C
    loop by returning to the calling program. The last value of ending
    radius has been assigned as the solution.
```

```
Function = Ending Radius*(Ending Radius*(A*Ending Radius - B)) - C
    Derivative of Function =
       Ending Radius*(Ending Radius*3.0*A - 2.0*B)
    DO I = 1,100
       IF((((Ending Radius-Radius at High Bound)*
          Derivative of Function-Function) *
          ((Ending Radius-Radius at Low Bound) *
          Derivative of Function-Function).GE.0.0) .OR.
          (ABS(2.0*Function).GT.
          (ABS(Last Diff Change*Derivative of Function)))) THEN
          Last Diff Change = Differential Change
          Differential_Change = 0.5*(Radius_at_High_Bound -
             Radius at Low Bound)
          Ending Radius = Radius at Low Bound + Differential Change
          IF (Radius at Low Bound .EQ. Ending Radius) RETURN
       ELSE
          Last Diff Change = Differential Change
          Differential Change = Function/Derivative of Function
          Last Ending Radius = Ending Radius
          Ending_Radius = Ending_Radius - Differential_Change
          IF (Last_Ending_Radius .EQ. Ending_Radius) RETURN
       IF (ABS(Differential Change) .LT. 1.0E-12) RETURN
       Function =
          Ending Radius* (Ending Radius* (A*Ending Radius - B)) - C
       Derivative of Function =
          Ending Radius*(Ending Radius*3.0*A - 2.0*B)
       IF (Function .LT. 0.0) THEN
          Radius at Low Bound = Ending Radius
          Radius at High Bound = Ending Radius
       END IF
    END DO
    PRINT *, 'ERROR! ROOT SEARCH EXCEEDED MAXIMUM ITERATIONS'
END OF SUBROUTINE
C-----
    SUBROUTINE GAS LOADINGS CONSTANT DEPTH
С
    Purpose: This subprogram applies the Haldane equation to update the
C
    gas loadings (partial pressures of helium and nitrogen) in the half-time
   compartments for a segment at constant depth.
SUBROUTINE GAS LOADINGS CONSTANT DEPTH (Depth,
                                 Run Time End of Segment)
    IMPLICIT NONE
ARGUMENTS
REAL Depth, Run Time End of Segment
LOCAL VARIABLES
```

```
INTEGER I
                                                  !loop counter
    INTEGER Last Segment Number
    REAL Initial Helium Pressure, Initial Nitrogen Pressure
    REAL Inspired Helium Pressure, Inspired Nitrogen Pressure
    REAL Ambient Pressure, Last Run Time
    REAL HALDANE EQUATION
                                            !function subprogram
GLOBAL CONSTANTS IN NAMED COMMON BLOCKS
REAL Water Vapor Pressure
    COMMON /Block 8/ Water Vapor Pressure
GLOBAL VARIABLES IN NAMED COMMON BLOCKS
INTEGER Segment Number
                                                   !both input
    REAL Run Time, Segment Time
                                                   !and output
    COMMON /Block_2/ Run_Time, Segment_Number, Segment Time
    REAL Ending Ambient Pressure
                                                      !output
    COMMON /Block 4/ Ending Ambient Pressure
    INTEGER Mix Number
    COMMON /Block 9/ Mix Number
    REAL Barometric Pressure
    COMMON /Block 18/ Barometric Pressure
GLOBAL ARRAYS IN NAMED COMMON BLOCKS
C-----
    REAL Helium Time Constant (16)
    COMMON /Block 1A/ Helium Time Constant
    REAL Nitrogen Time Constant (16)
    COMMON /Block 1B/ Nitrogen Time Constant
    REAL Helium Pressure (16), Nitrogen Pressure (16)
                                                  !both input
    COMMON /Block 3/ Helium Pressure, Nitrogen Pressure
                                                  !and output
    REAL Fraction Helium(10), Fraction Nitrogen(10)
    COMMON /Block 5/ Fraction Helium, Fraction Nitrogen
CALCULATIONS
Segment_Time = Run_Time_End_of_Segment - Run_Time
    Last_Run_Time = Run_Time_End_of_Segment
    Run_Time = Last_Run_Time
    Last Segment Number = Segment Number
    Segment Number = Last Segment Number + 1
    Ambient Pressure = Depth + Barometric Pressure
    Inspired Helium Pressure = (Ambient Pressure -
          Water Vapor Pressure) *Fraction Helium (Mix Number)
    Inspired Nitrogen Pressure = (Ambient Pressure -
          Water Vapor Pressure) *Fraction Nitrogen (Mix Number)
    Ending Ambient Pressure = Ambient Pressure
    DO I = 1,16
       Initial Helium Pressure = Helium Pressure(I)
       Initial Nitrogen Pressure = Nitrogen Pressure(I)
       Helium Pressure(I) = HALDANE EQUATION
```

```
(Initial Helium Pressure, Inspired Helium Pressure,
        Helium Time Constant(I), Segment Time)
      Nitrogen Pressure(I) = HALDANE EQUATION
        (Initial_Nitrogen_Pressure, Inspired_Nitrogen_Pressure,
        Nitrogen Time Constant(I), Segment Time)
   END DO
END OF SUBROUTINE
END
SUBROUTINE NUCLEAR REGENERATION
C
   Purpose: This subprogram calculates the regeneration of VPM critical
C
   radii that takes place over the dive time. The regeneration time constant
   has a time scale of weeks so this will have very little impact on dives of
   normal length, but will have a major impact for saturation dives.
SUBROUTINE NUCLEAR REGENERATION (Dive Time)
   IMPLICIT NONE
C
   ARGUMENTS
C-----
   REAL Dive Time
C-----
   LOCAL VARIABLES
INTEGER I
   REAL Crushing Pressure Pascals He, Crushing Pressure Pascals N2
   REAL Ending Radius He, Ending Radius N2
   REAL Crush Pressure Adjust Ratio He
   REAL Crush Pressure Adjust Ratio N2
   REAL Adj Crush Pressure He Pascals, Adj Crush Pressure N2 Pascals
GLOBAL CONSTANTS IN NAMED COMMON BLOCKS
REAL Surface Tension Gamma, Skin Compression GammaC
   COMMON /Block 19/ Surface Tension Gamma, Skin Compression GammaC
   REAL Regeneration_Time_Constant
   COMMON /Block_22/ Regeneration_Time_Constant
GLOBAL VARIABLES IN NAMED COMMON BLOCKS
C-----
   REAL Units Factor
   COMMON /Block 16/ Units Factor
GLOBAL ARRAYS IN NAMED COMMON BLOCKS
REAL Adjusted Critical Radius He (16)
   REAL Adjusted Critical Radius N2(16)
   COMMON /Block 7/ Adjusted Critical Radius He,
             Adjusted Critical Radius N2
   REAL Max Crushing Pressure He(16), Max Crushing Pressure N2(16) !input
   COMMON /Block 10/ Max Crushing Pressure He,
              Max_Crushing_Pressure N2
   REAL Regenerated Radius He(16), Regenerated Radius N2(16)
                                            !output
```

```
COMMON /Block 24/ Regenerated Radius He, Regenerated Radius N2
     REAL Adjusted_Crushing_Pressure_He(16)
                                                                !output
     REAL Adjusted_Crushing_Pressure_N2(16)
     COMMON /Block_25/ Adjusted_Crushing_Pressure_He,
                   Adjusted_Crushing_Pressure_N2
CALCULATIONS
    First convert the maximum crushing pressure obtained for each compartment
    to Pascals. Next, compute the ending radius for helium and nitrogen
     critical nuclei in each compartment.
DO I = 1,16
        Crushing Pressure Pascals He =
            (Max Crushing Pressure He(I)/Units Factor) * 101325.0
        Crushing Pressure Pascals N2 =
            (Max Crushing Pressure N2(I)/Units Factor) * 101325.0
        Ending_Radius_He = 1.0/(Crushing_Pressure_Pascals_He/
            (2.0*(Skin Compression GammaC - Surface Tension Gamma)) +
            1.0/Adjusted Critical Radius He(I))
        Ending_Radius_N2 = 1.0/(Crushing_Pressure_Pascals_N2/
            (2.0*(Skin Compression GammaC - Surface Tension Gamma)) +
            1.0/Adjusted_Critical_Radius_N2(I))
C-----
    A "regenerated" radius for each nucleus is now calculated based on the
     regeneration time constant. This means that after application of
     crushing pressure and reduction in radius, a nucleus will slowly grow
С
С
     back to its original initial radius over a period of time. This
     phenomenon is probabilistic in nature and depends on absolute temperature.
     It is independent of crushing pressure.
Regenerated Radius He(I) = Adjusted Critical Radius He(I) +
            (Ending Radius He - Adjusted Critical Radius He(I)) *
            EXP(-Dive Time/Regeneration Time Constant)
        Regenerated Radius N2(I) = Adjusted Critical Radius N2(I) +
            (Ending Radius N2 - Adjusted Critical Radius N2(I)) *
            EXP(-Dive Time/Regeneration Time Constant)
C-----
     In order to preserve reference back to the initial critical radii after
     regeneration, an "adjusted crushing pressure" for the nuclei in each compartment must be computed. In other words, this is the value of
C
C
     crushing pressure that would have reduced the original nucleus to the
C
     to the present radius had regeneration not taken place. The ratio
C
     for adjusting crushing pressure is obtained from algebraic manipulation
C
     of the standard VPM equations. The adjusted crushing pressure, in lieu
С
     of the original crushing pressure, is then applied in the VPM Critical
     Volume Algorithm and the VPM Repetitive Algorithm.
C-----
        Crush Pressure Adjust Ratio He =
            (Ending Radius He*(Adjusted Critical Radius He(I) -
            Regenerated Radius He(I))) / (Regenerated Radius He(I) *
            (Adjusted_Critical_Radius_He(I) - Ending_Radius_He))
        Crush Pressure Adjust Ratio N2 =
            (Ending Radius N2*(Adjusted Critical Radius N2(I) -
            Regenerated Radius N2(I))) / (Regenerated Radius N2(I) *
            (Adjusted Critical Radius N2(I) - Ending Radius N2))
        Adj Crush Pressure He Pascals = Crushing Pressure Pascals He *
            Crush Pressure Adjust Ratio He
```

```
Adj Crush Pressure N2 Pascals = Crushing Pressure Pascals N2 *
         Crush Pressure Adjust Ratio N2
      Adjusted Crushing Pressure He(I) =
         (Adj Crush Pressure He Pascals / 101325.0) * Units Factor
      Adjusted Crushing Pressure N2(I) =
         (Adj Crush Pressure N2 Pascals / 101325.0) * Units Factor
    END DO
END OF SUBROUTINE
RETURN
    END
SUBROUTINE CALC INITIAL ALLOWABLE GRADIENT
С
    Purpose: This subprogram calculates the initial allowable gradients for
С
    helium and nitrogren in each compartment. These are the gradients that
С
    will be used to set the deco ceiling on the first pass through the deco
C
    loop. If the Critical Volume Algorithm is set to "off", then these
    gradients will determine the final deco schedule. Otherwise, if the
C
C
    Critical Volume Algorithm is set to "on", these gradients will be further
C
    "relaxed" by the Critical Volume Algorithm subroutine. The initial
С
    allowable gradients are referred to as "PssMin" in the papers by Yount
С
    and colleauges, i.e., the minimum supersaturation pressure gradients
    that will probe bubble formation in the VPM nuclei that started with the
С
С
    designated minimum initial radius (critical radius).
С
С
    The initial allowable gradients are computed directly from the
    "regenerated" radii after the Nuclear Regeneration subroutine.
    gradients are tracked separately for helium and nitrogen.
SUBROUTINE CALC INITIAL ALLOWABLE GRADIENT
    IMPLICIT NONE
LOCAL VARIABLES
INTEGER I
                                              !loop counter
    REAL Initial Allowable Grad He Pa, Initial Allowable Grad N2 Pa
GLOBAL CONSTANTS IN NAMED COMMON BLOCKS
REAL Surface_Tension_Gamma, Skin_Compression_GammaC
    COMMON /Block 19/ Surface Tension Gamma, Skin Compression GammaC
GLOBAL VARIABLES IN NAMED COMMON BLOCKS
REAL Units Factor
    COMMON /Block 16/ Units Factor
C-----
   GLOBAL ARRAYS IN NAMED COMMON BLOCKS
REAL Regenerated Radius He(16), Regenerated Radius N2(16)
    COMMON /Block 24/ Regenerated_Radius_He, Regenerated_Radius_N2
    REAL Allowable Gradient He(16), Allowable Gradient N2 (16)
                                                  !output
    COMMON /Block 26/ Allowable Gradient He, Allowable Gradient N2
    REAL Initial Allowable Gradient He (16)
                                                  !output
```

```
REAL Initial Allowable Gradient N2(16)
    COMMON /Block 27/
     Initial_Allowable_Gradient_He, Initial_Allowable_Gradient_N2
CALCULATIONS
С
    The initial allowable gradients are computed in Pascals and then converted
С
    to the diving pressure units. Two different sets of arrays are used to
С
    save the calculations - Initial Allowable Gradients and Allowable
С
    Gradients. The Allowable Gradients are assigned the values from Initial
С
   Allowable Gradients however the Allowable Gradients can be changed later
C
   by the Critical Volume subroutine. The values for the Initial Allowable
С
    Gradients are saved in a global array for later use by both the Critical
   Volume subroutine and the VPM Repetitive Algorithm subroutine.
DO I = 1,16
       Initial Allowable Grad N2 Pa = ((2.0*Surface Tension Gamma*
          (Skin Compression GammaC - Surface Tension Gamma)) /
          (Regenerated Radius N2(I)*Skin Compression GammaC))
       Initial Allowable Grad He Pa = ((2.0*Surface Tension Gamma*
          (Skin Compression GammaC - Surface Tension Gamma) /
          (Regenerated Radius He(I)*Skin Compression GammaC))
       Initial Allowable Gradient N2(I) =
          (Initial Allowable Grad N2 Pa / 101325.0) * Units Factor
       Initial Allowable Gradient He(I) =
          (Initial Allowable Grad He Pa / 101325.0) * Units Factor
       Allowable Gradient He(I) = Initial Allowable Gradient He(I)
       Allowable Gradient N2(I) = Initial Allowable Gradient N2(I)
END OF SUBROUTINE
RETURN
    END
SUBROUTINE CALC DECO CEILING
    Purpose: This subprogram calculates the deco ceiling (the safe ascent
    depth) in each compartment, based on the allowable gradients, and then
    finds the deepest deco ceiling across all compartments. This deepest
    value (Deco Ceiling Depth) is then used by the Decompression Stop
    subroutine to determine the actual deco schedule.
SUBROUTINE CALC DECO CEILING (Deco Ceiling Depth)
    IMPLICIT NONE
C-----
   ARGUMENTS
REAL Deco Ceiling Depth
   LOCAL VARIABLES
INTEGER I
                                               !loop counter
    REAL Gas Loading, Weighted Allowable Gradient
    REAL Tolerated Ambient Pressure
LOCAL ARRAYS
```

```
REAL Compartment Deco Ceiling(16)
GLOBAL CONSTANTS IN NAMED COMMON BLOCKS
REAL Constant Pressure Other Gases
    COMMON /Block_17/ Constant_Pressure Other Gases
GLOBAL VARIABLES IN NAMED COMMON BLOCKS
REAL Barometric Pressure
    COMMON /Block 18/ Barometric Pressure
C-----
    GLOBAL ARRAYS IN NAMED COMMON BLOCKS
REAL Helium Pressure (16), Nitrogen Pressure (16)
    COMMON /Block 3/ Helium Pressure, Nitrogen Pressure
    REAL Allowable Gradient He(16), Allowable Gradient N2 (16)
                                                    !input
    COMMON /Block 26/ Allowable Gradient He, Allowable Gradient N2
CALCULATIONS
    Since there are two sets of allowable gradients being tracked, one for
C
    helium and one for nitrogen, a "weighted allowable gradient" must be
C
    computed each time based on the proportions of helium and nitrogen in
    each compartment. This proportioning follows the methodology of
C
C
    Buhlmann/Keller. If there is no helium and nitrogen in the compartment,
C
    such as after extended periods of oxygen breathing, then the minimum value
C
    across both gases will be used. It is important to note that if a
C
    compartment is empty of helium and nitrogen, then the weighted allowable
    gradient formula cannot be used since it will result in division by zero.
Gas Loading = Helium Pressure(I) + Nitrogen Pressure(I)
    IF (Gas Loading .GT. 0.0) THEN
       Weighted Allowable Gradient =
       (Allowable Gradient He(I) * Helium Pressure(I) +
       Allowable_Gradient_N2(I) * Nitrogen_Pressure(I)) /
       (Helium Pressure(I) + Nitrogen Pressure(I))
       Tolerated Ambient Pressure = (Gas Loading +
       Constant_Pressure_Other_Gases) - Weighted_Allowable_Gradient
    ELSE
       Weighted Allowable Gradient =
       MIN(Allowable Gradient He(I), Allowable Gradient N2(I))
       Tolerated Ambient Pressure =
       Constant Pressure Other Gases - Weighted Allowable Gradient
    END IF
The tolerated ambient pressure cannot be less than zero absolute, i.e.,
    the vacuum of outer space!
IF (Tolerated Ambient Pressure .LT. 0.0) THEN
       Tolerated Ambient Pressure = 0.0
The Deco Ceiling Depth is computed in a loop after all of the individual
C
    compartment deco ceilings have been calculated. It is important that the
С
    Deco Ceiling Depth (max deco ceiling across all compartments) only be
С
    extracted from the compartment values and not be compared against some
    initialization value. For example, if MAX(Deco Ceiling Depth . .) was
```

```
compared against zero, this could cause a program lockup because sometimes
C
    the Deco Ceiling Depth needs to be negative (but not less than zero
C
    absolute ambient pressure) in order to decompress to the last stop at zero
C
    depth.
Compartment Deco Ceiling(I) =
         Tolerated Ambient Pressure - Barometric Pressure
    END DO
    Deco Ceiling Depth = Compartment Deco Ceiling(1)
    DO I = 2,16
      Deco Ceiling Depth =
         MAX(Deco Ceiling Depth, Compartment Deco Ceiling(I))
    END DO
END OF SUBROUTINE
RETURN
    END
SUBROUTINE CALC MAX ACTUAL GRADIENT
С
    Purpose: This subprogram calculates the actual supersaturation gradient
C
    obtained in each compartment as a result of the ascent profile during
    decompression. Similar to the concept with crushing pressure, the
C
С
    supersaturation gradients are not cumulative over a multi-level, staged
С
    ascent. Rather, it will be the maximum value obtained in any one discrete
С
    step of the overall ascent. Thus, the program must compute and store the
С
    maximum actual gradient for each compartment that was obtained across all
С
    steps of the ascent profile. This subroutine is invoked on the last pass
С
    through the deco stop loop block when the final deco schedule is being
С
    generated.
С
C
    The max actual gradients are later used by the VPM Repetitive Algorithm to
C
    determine if adjustments to the critical radii are required. If the max
С
    actual gradient did not exceed the initial alllowable gradient, then no
С
    adjustment will be made. However, if the max actual gradient did exceed
C
    the intitial allowable gradient, such as permitted by the Critical Volume
C
    Algorithm, then the critical radius will be adjusted (made larger) on the
C
    repetitive dive to compensate for the bubbling that was allowed on the
С
    previous dive. The use of the max actual gradients is intended to prevent
    the repetitive algorithm from being overly conservative.
SUBROUTINE CALC MAX ACTUAL GRADIENT (Deco Stop Depth)
    IMPLICIT NONE
ARGUMENTS
C-----
   REAL Deco Stop Depth
LOCAL VARIABLES
REAL Compartment Gradient
C-----
   GLOBAL CONSTANTS IN NAMED COMMON BLOCKS
REAL Constant Pressure Other Gases
    COMMON /Block 17/ Constant Pressure Other Gases
GLOBAL VARIABLES IN NAMED COMMON BLOCKS
```

```
REAL Barometric Pressure
   COMMON /Block 18/ Barometric Pressure
GLOBAL ARRAYS IN NAMED COMMON BLOCKS
REAL Helium Pressure (16), Nitrogen Pressure (16)
                                             !input
   COMMON /Block 3/ Helium Pressure, Nitrogen Pressure
   REAL Max Actual Gradient (16)
   COMMON /Block 12/ Max Actual Gradient
CALCULATIONS
   Note: negative supersaturation gradients are meaningless for this
   application, so the values must be equal to or greater than zero.
DO I = 1,16
      Compartment Gradient = (Helium Pressure(I) +
        Nitrogen Pressure(I) + Constant Pressure Other Gases)
        - (Deco Stop Depth + Barometric Pressure)
      IF (Compartment_Gradient .LE. 0.0) THEN
        Compartment Gradient = 0.0
      END IF
      Max Actual Gradient(I) =
        MAX(Max Actual Gradient(I), Compartment Gradient)
   END DO
END OF SUBROUTINE
RETURN
   END
SUBROUTINE CALC SURFACE PHASE VOLUME TIME
C
   Purpose: This subprogram computes the surface portion of the total phase
С
   volume time. This is the time factored out of the integration of
C
   supersaturation gradient x time over the surface interval. The VPM
C
   considers the gradients that allow bubbles to form or to drive bubble
C
   growth both in the water and on the surface after the dive.
C
C
   This subroutine is a new development to the VPM algorithm in that it
C
   computes the time course of supersaturation gradients on the surface
С
   when both helium and nitrogen are present. Refer to separate write-up
   for a more detailed explanation of this algorithm.
SUBROUTINE CALC_SURFACE_PHASE_VOLUME_TIME
   IMPLICIT NONE
C-----
   LOCAL VARIABLES
C-----
   REAL Integral_Gradient_x_Time, Decay_Time_to_Zero_Gradient
   REAL Surface Inspired N2 Pressure
GLOBAL CONSTANTS IN NAMED COMMON BLOCKS
REAL Water Vapor Pressure
   COMMON /Block 8/ Water Vapor Pressure
GLOBAL VARIABLES IN NAMED COMMON BLOCKS
REAL Barometric Pressure
```

```
COMMON /Block 18/ Barometric Pressure
GLOBAL ARRAYS IN NAMED COMMON BLOCKS
REAL Helium Time Constant (16)
    COMMON /Block 1A/ Helium Time Constant
    REAL Nitrogen Time Constant (16)
    COMMON /Block 1B/ Nitrogen Time Constant
    REAL Helium Pressure (16), Nitrogen Pressure (16)
                                                          !input
    COMMON /Block 3/ Helium Pressure, Nitrogen Pressure
    REAL Surface Phase Volume Time (16)
                                                         !output
    COMMON /Block 11/ Surface Phase Volume Time
CALCULATIONS
Surface Inspired N2 Pressure = (Barometric Pressure -
          Water Vapor Pressure) *0.79
    DO I = 1,16
       IF (Nitrogen Pressure(I) .GT. Surface Inspired N2 Pressure)
           Surface_Phase_Volume_Time(I) =
              (Helium_Pressure(I)/Helium_Time_Constant(I)+
              (Nitrogen Pressure(I)-Surface Inspired N2 Pressure)/
              Nitrogen Time Constant(I))
              /(Helium Pressure(I) + Nitrogen Pressure(I) -
              Surface Inspired N2 Pressure)
       ELSE IF ((Nitrogen Pressure(I) .LE.
              Surface Inspired N2 Pressure).AND.
              (Helium Pressure(I)+Nitrogen Pressure(I).GE.
              Surface Inspired N2 Pressure)) THEN
          Decay Time to Zero Gradient =
             1.0/(Nitrogen Time Constant(I)-Helium_Time_Constant(I))
             *ALOG((Surface Inspired N2 Pressure -
             Nitrogen Pressure(I))/Helium Pressure(I))
           Integral Gradient x Time =
              Helium Pressure(I)/Helium Time Constant(I)*
              (1.0-EXP(-Helium_Time_Constant(I)*
              Decay Time to Zero Gradient))+
              (Nitrogen_Pressure(I)-Surface_Inspired_N2_Pressure)/
              Nitrogen_Time_Constant(I)*
              (1.0-EXP(-Nitrogen_Time_Constant(I)*
              Decay_Time_to_Zero_Gradient))
           Surface Phase Volume Time(I) =
              Integral_Gradient_x_Time/(Helium_Pressure(I) +
              Nitrogen Pressure(I) - Surface Inspired N2 Pressure)
       ELSE
           Surface Phase Volume Time(I) = 0.0
    END DO
END OF SUBROUTINE
RETURN
    END
```

C=====================================	
SUBROUTINE CRITICAL_VOLUME (Deco_Phase_Volume_Time)	========
IMPLICIT NONE	
C ARGUMENTS	=========
C=====================================	!input
C LOCAL VARIABLES	========
C=====================================	!loop counter
REAL Parameter_Lambda_Pascals REAL Adj_Crush_Pressure_He_Pascals, Adj_Crush_Pressure_N2_Pa REAL Initial_Allowable_Grad_He_Pa, Initial_Allowable_Grad_N2 REAL New_Allowable_Grad_He_Pascals, New_Allowable_Grad_N2_Pa REAL B, C	2_Pa
C LOCAL ARRAYS	=========
C=====================================	========
C=====================================	=========
C GLOBAL CONSTANTS IN NAMED COMMON BLOCKS C===================================	=========
REAL Surface_Tension_Gamma, Skin_Compression_GammaC COMMON /Block_19/ Surface_Tension_Gamma, Skin_Compression_Ga	ammaC
REAL Crit_Volume_Parameter_Lambda COMMON /Block_20/ Crit_Volume_Parameter_Lambda C===================================	
C GLOBAL VARIABLES IN NAMED COMMON BLOCKS	
C=====================================	========
C=====================================	========
C=====================================	======== !input
REAL Surface_Phase_Volume_Time(16) COMMON /Block_11/ Surface_Phase_Volume_Time	!input
REAL Adjusted_Crushing_Pressure_He(16) REAL Adjusted_Crushing_Pressure_N2(16) COMMON /Block_25/ Adjusted_Crushing_Pressure_He, * Adjusted_Crushing_Pressure_N2	!input
REAL Allowable_Gradient_He(16), Allowable_Gradient_N2 (16) COMMON /Block_26/ Allowable_Gradient_He, Allowable_Gradient_	!output _N2
REAL Initial_Allowable_Gradient_He(16) REAL Initial_Allowable_Gradient_N2(16) COMMON /Block_27/ * Initial_Allowable_Gradient_He, Initial_Allowable_Gradient_C====================================	!input nt_N2 ========

```
CALCULATIONS
C
     Note: Since the Critical Volume Parameter Lambda was defined in units of
С
     fsw-min in the original papers by Yount and colleauges, the same
     convention is retained here. Although Lambda is adjustable only in units
С
С
     of fsw-min in the program settings (range from 6500 to 8300 with default
С
     7500), it will convert to the proper value in Pascals-min in this
С
     subroutine regardless of which diving pressure units are being used in
С
     the main program - feet of seawater (fsw) or meters of seawater (msw).
С
     The allowable gradient is computed using the quadratic formula (refer to
     separate write-up posted on the Deco List web site).
Parameter Lambda Pascals = (Crit Volume Parameter Lambda/33.0)
                                 * 101325.0
     DO I = 1,16
         Phase Volume Time(I) = Deco Phase Volume Time +
             Surface_Phase_Volume_Time(I)
     END DO
     DO I = 1,16
         Adj Crush Pressure He Pascals =
             (Adjusted Crushing Pressure He(I)/Units Factor) * 101325.0
         Initial Allowable Grad He Pa =
             (Initial Allowable Gradient He(I)/Units Factor) * 101325.0
         B = Initial_Allowable_Grad_He_Pa +
              (Parameter_Lambda_Pascals*Surface_Tension_Gamma)/
             (Skin Compression GammaC*Phase Volume Time(I))
         C = (Surface Tension Gamma*(Surface Tension Gamma*
             (Parameter Lambda Pascals*
             Adj Crush Pressure He Pascals)))
             /(Skin Compression GammaC*(Skin Compression GammaC*
             Phase Volume Time(I)))
         New Allowable Grad He Pascals = (B + SQRT(B**2)
             -4.0*C))/2.0
         Allowable Gradient He(I) =
             (New Allowable Grad He Pascals/101325.0) *Units Factor
     END DO
     DO I = 1,16
         Adj Crush Pressure N2 Pascals =
             (Adjusted Crushing Pressure N2(I)/Units Factor) * 101325.0
         Initial Allowable Grad N2 Pa =
             (Initial Allowable Gradient N2(I)/Units Factor) * 101325.0
         B = Initial Allowable Grad N2 Pa +
             (Parameter_Lambda_Pascals*Surface_Tension Gamma)/
             (Skin Compression GammaC*Phase Volume Time(I))
         C = (Surface Tension Gamma*(Surface Tension Gamma*
             (Parameter Lambda Pascals*
             Adj Crush Pressure N2_Pascals)))
             /(Skin Compression GammaC*(Skin Compression GammaC*
             Phase Volume Time(I)))
         New Allowable Grad N2 Pascals = (B + SQRT(B**2))
             -4.0*C))/2.0
         Allowable Gradient_N2(I) =
              (New Allowable Grad N2 Pascals/101325.0) *Units Factor
```



```
REAL Helium Pressure (16), Nitrogen Pressure (16)
     COMMON /Block 3/ Helium Pressure, Nitrogen Pressure
     REAL Fraction Helium(10), Fraction Nitrogen(10)
     COMMON /Block 5/ Fraction Helium, Fraction Nitrogen
C
    CALCULATIONS
C
    First initialize some variables
Depth Start of Deco Zone = 0.0
     Starting Ambient Pressure = Starting Depth + Barometric Pressure
    Initial Inspired He Pressure = (Starting Ambient Pressure -
            Water Vapor Pressure) *Fraction Helium (Mix Number)
    Initial Inspired N2 Pressure = (Starting Ambient Pressure -
            Water Vapor Pressure) *Fraction Nitrogen (Mix Number)
     Helium Rate = Rate * Fraction Helium(Mix Number)
    Nitrogen Rate = Rate * Fraction Nitrogen(Mix Number)
ESTABLISH THE BOUNDS FOR THE ROOT SEARCH USING THE BISECTION METHOD
     AND CHECK TO MAKE SURE THAT THE ROOT WILL BE WITHIN BOUNDS. PROCESS
C
     EACH COMPARTMENT INDIVIDUALLY AND FIND THE MAXIMUM DEPTH ACROSS ALL
С
    COMPARTMENTS (LEADING COMPARTMENT)
С
    In this case, we are solving for time - the time when the gas tension in
C
    the compartment will be equal to ambient pressure. The low bound for time
С
    is set at zero and the high bound is set at the time it would take to
С
    ascend to zero ambient pressure (absolute). Since the ascent rate is
С
    negative, a multiplier of -1.0 is used to make the time positive. The
С
    desired point when gas tension equals ambient pressure is found at a time
С
     somewhere between these endpoints. The algorithm checks to make sure that
    the solution lies in between these bounds by first computing the low bound
    and high bound function values.
Low Bound = 0.0
    High Bound = -1.0*(Starting Ambient Pressure/Rate)
     DO 200 I = 1,16
        Initial Helium Pressure = Helium Pressure(I)
        Initial Nitrogen Pressure = Nitrogen Pressure(I)
        Function at Low Bound = Initial Helium Pressure +
            Initial Nitrogen Pressure + Constant Pressure Other Gases
            - Starting Ambient Pressure
        High Bound Helium Pressure = SCHREINER EQUATION
            (Initial Inspired He Pressure, Helium Rate,
            High_Bound, Helium_Time_Constant(I),
            Initial Helium Pressure)
        High_Bound_Nitrogen_Pressure = SCHREINER EQUATION
            (Initial Inspired N2 Pressure, Nitrogen Rate,
            High Bound, Nitrogen Time Constant(I),
            Initial Nitrogen Pressure)
        Function at High Bound = High Bound Helium Pressure +
            High Bound Nitrogen Pressure+Constant Pressure Other Gases
        IF ((Function at High Bound * Function at Low Bound) .GE. 0.0)
                                                          THEN
            PRINT *, 'ERROR! ROOT IS NOT WITHIN BRACKETS'
            PAUSE
        END IF
```

```
APPLY THE BISECTION METHOD IN SEVERAL ITERATIONS UNTIL A SOLUTION WITH
    THE DESIRED ACCURACY IS FOUND
C
    Note: the program allows for up to 100 iterations. Normally an exit will
C
    be made from the loop well before that number. If, for some reason, the
C
    program exceeds 100 iterations, there will be a pause to alert the user.
IF (Function at Low Bound .LT. 0.0) THEN
           Time to Start of Deco Zone = Low Bound
           Differential Change = High Bound - Low Bound
       ELSE
           Time to Start of Deco Zone = High Bound
          Differential Change = Low Bound - High Bound
       DO 150 J = 1, 100
          Last Diff_Change = Differential_Change
          Differential_Change = Last_Diff_Change*0.5
          Mid Range Time = Time to Start of Deco Zone +
                        Differential Change
          Mid Range Helium Pressure = SCHREINER EQUATION
              (Initial Inspired He Pressure, Helium Rate,
              Mid_Range_Time, Helium_Time_Constant(I),
              Initial Helium Pressure)
          Mid Range Nitrogen Pressure = SCHREINER EQUATION
              (Initial Inspired N2 Pressure, Nitrogen Rate,
              Mid Range Time, Nitrogen Time Constant(I),
              Initial Nitrogen Pressure)
           Function at Mid Range =
              Mid Range Helium Pressure +
              Mid Range Nitrogen Pressure +
              Constant Pressure Other Gases -
              (Starting Ambient Pressure + Rate*Mid Range Time)
           IF (Function at Mid Range .LE. 0.0)
              Time to Start of Deco Zone = Mid Range Time
           IF ((ABS(Differential Change) .LT. 1.0E-3) .OR.
              (Function at_Mid_Range .EQ. 0.0)) GOTO 170
150
       CONTINUE
       PRINT *, 'ERROR! ROOT SEARCH EXCEEDED MAXIMUM ITERATIONS'
When a solution with the desired accuracy is found, the program jumps out
    of the loop to Line 170 and assigns the solution value for the individual
C
C
    compartment.
Cpt_Depth_Start_of_Deco_Zone = (Starting_Ambient Pressure +
          Rate*Time to Start of Deco Zone) - Barometric Pressure
The overall solution will be the compartment with the maximum depth where
    gas tension equals ambient pressure (leading compartment).
Depth Start of Deco Zone = MAX(Depth Start of Deco Zone,
           Cpt_Depth_Start_of Deco Zone)
   CONTINUE
END OF SUBROUTINE
RETURN
    END
```

```
SUBROUTINE PROJECTED ASCENT
C
   Purpose: This subprogram performs a simulated ascent outside of the main
   program to ensure that a deco ceiling will not be violated due to unusual
C
   gas loading during ascent (on-gassing). If the deco ceiling is violated,
C
   the stop depth will be adjusted deeper by the step size until a safe
C
C
   ascent can be made.
SUBROUTINE PROJECTED ASCENT (Starting Depth, Rate,
                     Deco Stop Depth, Step Size)
   IMPLICIT NONE
ARGUMENTS
REAL Starting Depth, Rate, Step Size
   REAL Deco Stop Depth
                                  !input and output
C-----
   LOCAL VARIABLES
INTEGER I
                                         !loop counter
   REAL Initial Inspired He Pressure, Initial Inspired N2 Pressure
   REAL Helium_Rate, Nitrogen_Rate
   REAL Starting Ambient Pressure, Ending Ambient Pressure
   REAL New_Ambient_Pressure, Segment_Time
REAL Temp_Helium_Pressure, Temp_Nitrogen_Pressure
   REAL Weighted Allowable Gradient
   REAL SCHREINER EQUATION
                                     !function subprogram
LOCAL ARRAYS
REAL Initial Helium Pressure (16), Initial Nitrogen Pressure (16)
   REAL Temp Gas Loading (16), Allowable Gas Loading (16)
GLOBAL CONSTANTS IN NAMED COMMON BLOCKS
REAL Water Vapor Pressure
   COMMON /Block 8/ Water Vapor Pressure
   REAL Constant Pressure Other Gases
   COMMON /Block 17/ Constant Pressure Other Gases
GLOBAL VARIABLES IN NAMED COMMON BLOCKS
INTEGER Mix Number
   COMMON /Block 9/ Mix Number
   REAL Barometric Pressure
   COMMON /Block 18/ Barometric Pressure
GLOBAL ARRAYS IN NAMED COMMON BLOCKS
REAL Helium Time Constant (16)
   COMMON /Block 1A/ Helium Time Constant
   REAL Nitrogen Time Constant (16)
   COMMON /Block 1B/ Nitrogen Time Constant
   REAL Helium Pressure (16), Nitrogen Pressure (16)
                                              !input
   COMMON /Block 3/ Helium Pressure, Nitrogen Pressure
   REAL Fraction Helium(10), Fraction Nitrogen(10)
   COMMON /Block 5/ Fraction Helium, Fraction Nitrogen
```

```
REAL Allowable Gradient He(16), Allowable Gradient N2 (16)
                                                                !input
     COMMON /Block 26/ Allowable Gradient He, Allowable Gradient N2
CALCULATIONS
New Ambient Pressure = Deco Stop Depth + Barometric Pressure
     Starting Ambient Pressure = Starting Depth + Barometric Pressure
     Initial Inspired He Pressure = (Starting Ambient Pressure -
           Water Vapor Pressure) *Fraction Helium (Mix Number)
     Initial Inspired N2 Pressure = (Starting Ambient Pressure -
           Water Vapor Pressure) *Fraction Nitrogen (Mix Number)
     Helium Rate = Rate * Fraction Helium(Mix Number)
     Nitrogen_Rate = Rate * Fraction_Nitrogen(Mix_Number)
     DO I = 1,16
        Initial Helium Pressure(I) = Helium Pressure(I)
        Initial Nitrogen Pressure(I) = Nitrogen Pressure(I)
     END DO
665
     Ending Ambient Pressure = New Ambient Pressure
     Segment Time = (Ending Ambient Pressure -
        Starting Ambient Pressure)/Rate
     DO 670 I = 1,16
        Temp Helium Pressure = SCHREINER EQUATION
            (Initial Inspired He Pressure, Helium Rate,
            Segment Time, Helium Time Constant(I),
            Initial Helium Pressure(I))
        Temp Nitrogen Pressure = SCHREINER EQUATION
            (Initial Inspired N2 Pressure, Nitrogen Rate,
            Segment Time, Nitrogen Time Constant(I),
            Initial Nitrogen Pressure(I))
        Temp Gas Loading(I) = Temp Helium Pressure +
            Temp Nitrogen Pressure
     IF (Temp Gas Loading(I) .GT. 0.0) THEN
        Weighted Allowable Gradient =
        (Allowable_Gradient_He(I) * Temp_Helium_Pressure +
        Allowable_Gradient_N2(I) * Temp_Nitrogen_Pressure) /
        Temp Gas Loading(I)
     ELSE
        Weighted Allowable Gradient =
        MIN(Allowable Gradient He(I), Allowable Gradient N2(I))
     END IF
        Allowable Gas Loading(I) = Ending Ambient Pressure +
           Weighted Allowable Gradient - Constant Pressure Other Gases
670
    CONTINUE
     DO 671 I = 1,16
        IF (Temp Gas Loading(I) .GT. Allowable Gas Loading(I)) THEN
            New Ambient Pressure = Ending Ambient Pressure + Step Size
            Deco Stop Depth = Deco Stop Depth + Step Size
            GOTO 665
        END IF
   CONTINUE
END OF SUBROUTINE
RETURN
```

END

```
SUBROUTINE DECOMPRESSION STOP
C
   Purpose: This subprogram calculates the required time at each
C
   decompression stop.
SUBROUTINE DECOMPRESSION STOP (Deco Stop Depth, Step Size)
   IMPLICIT NONE
ARGUMENTS
REAL Deco Stop Depth, Step Size
LOCAL VARIABLES
CHARACTER OS Command*3
   INTEGER I
                                     !loop counter
   INTEGER Last Segment Number
   REAL Ambient Pressure
   REAL Inspired Helium Pressure, Inspired Nitrogen Pressure
   REAL Last_Run_Time
   REAL Deco Ceiling Depth, Next Stop
   REAL Round_Up_Operation, Temp_Segment_Time, Time_Counter
   REAL Weighted Allowable Gradient
   REAL HALDANE EQUATION
                                 !function subprogram
LOCAL ARRAYS
C-----
   REAL Initial Helium Pressure(16)
   REAL Initial Nitrogen Pressure (16)
GLOBAL CONSTANTS IN NAMED COMMON BLOCKS
REAL Water Vapor Pressure
   COMMON /Block 8/ Water Vapor Pressure
   REAL Constant Pressure Other Gases
   COMMON /Block 17/ Constant Pressure Other Gases
   REAL Minimum_Deco_Stop_Time
   COMMON /Block_21/ Minimum_Deco_Stop_Time
GLOBAL VARIABLES IN NAMED COMMON BLOCKS
INTEGER Segment Number
   REAL Run Time, Segment_Time
   COMMON /Block 2/ Run Time, Segment Number, Segment Time
   REAL Ending Ambient Pressure
   COMMON /Block 4/ Ending Ambient Pressure
   INTEGER Mix Number
   COMMON /Block 9/ Mix Number
   REAL Barometric Pressure
   COMMON /Block 18/ Barometric Pressure
GLOBAL ARRAYS IN NAMED COMMON BLOCKS
```

```
REAL Helium Time Constant (16)
    COMMON /Block 1A/ Helium Time Constant
    REAL Nitrogen_Time Constant(16)
    COMMON /Block 1B/ Nitrogen Time Constant
    REAL Helium Pressure (16), Nitrogen Pressure (16)
                                                         !both input
    COMMON /Block_3/ Helium_Pressure, Nitrogen Pressure
                                                         !and output
    REAL Fraction Helium(10), Fraction Nitrogen(10)
    COMMON /Block 5/ Fraction Helium, Fraction Nitrogen
    REAL Allowable Gradient He(16), Allowable Gradient N2 (16)
                                                              !input
    COMMON /Block 26/ Allowable Gradient He, Allowable Gradient N2
CALCULATIONS
OS Command = 'CLS'
    Last Run Time = Run Time
    Round_Up_Operation = ANINT((Last_Run_Time/Minimum_Deco_Stop_Time)
                            + 0.5) * Minimum Deco Stop Time
    Segment Time = Round Up Operation - Run Time
    Run_Time = Round_Up_Operation
    Temp_Segment_Time = Segment_Time
    Last_Segment_Number = Segment_Number
    Segment Number = Last Segment Number + 1
    Ambient Pressure = Deco Stop Depth + Barometric Pressure
    Ending Ambient Pressure = Ambient Pressure
    Next Stop = Deco Stop Depth - Step Size
    Inspired Helium Pressure = (Ambient Pressure -
        Water Vapor Pressure) *Fraction Helium (Mix Number)
    Inspired Nitrogen Pressure = (Ambient Pressure -
       Water Vapor Pressure) *Fraction Nitrogen (Mix Number)
Check to make sure that program won't lock up if unable to decompress
    to the next stop. If so, write error message and terminate program.
DO I = 1,16
    IF ((Inspired Helium Pressure + Inspired Nitrogen Pressure)
                                               .GT. 0.0) THEN
        Weighted Allowable Gradient =
        (Allowable_Gradient_He(I) * Inspired_Helium_Pressure +
        Allowable_Gradient_N2(I) * Inspired_Nitrogen_Pressure) /
        (Inspired_Helium_Pressure + Inspired_Nitrogen_Pressure)
        IF ((Inspired Helium Pressure + Inspired Nitrogen Pressure +
          Constant Pressure Other Gases - Weighted Allowable Gradient)
          .GT. (Next Stop + Barometric Pressure)) THEN
           CALL SYSTEMQQ (OS Command)
           WRITE (*,905) Deco_Stop_Depth
           WRITE (*,906)
           WRITE (*,907)
           STOP 'PROGRAM TERMINATED'
        END IF
    END IF
    END DO
    DO 720 I = 1,16
700
        Initial Helium Pressure(I) = Helium Pressure(I)
        Initial Nitrogen Pressure(I) = Nitrogen Pressure(I)
```

```
Helium Pressure(I) = HALDANE EQUATION
     (Initial Helium Pressure(I), Inspired Helium Pressure,
     Helium_Time_Constant(I), Segment_Time)
     Nitrogen Pressure(I) = HALDANE EQUATION
     (Initial_Nitrogen_Pressure(I), Inspired_Nitrogen_Pressure,
     Nitrogen Time Constant(I), Segment Time)
   CONTINUE
720
   CALL CALC DECO CEILING (Deco Ceiling Depth)
   IF (Deco Ceiling Depth .GT. Next Stop) THEN
      Segment Time = Minimum Deco Stop Time
      Time Counter = Temp Segment Time
      Temp Segment Time = Time_Counter + Minimum_Deco_Stop_Time
      Last Run Time = Run Time
      Run_Time = Last_Run_Time + Minimum_Deco_Stop_Time
      GOTO 700
   END IF
   Segment Time = Temp Segment Time
FORMAT STATEMENTS - ERROR MESSAGES
FORMAT ('OERROR! OFF-GASSING GRADIENT IS TOO SMALL TO DECOMPRESS'
  *1X,'AT THE',F6.1,1X,'STOP')
906
  FORMAT ('OREDUCE STEP SIZE OR INCREASE OXYGEN FRACTION')
907 FORMAT ('')
C-----
  END OF SUBROUTINE
SUBROUTINE GAS LOADINGS SURFACE INTERVAL
   Purpose: This subprogram calculates the gas loading (off-gassing) during
   a surface interval.
SUBROUTINE GAS LOADINGS SURFACE INTERVAL (Surface Interval Time)
   IMPLICIT NONE
ARGUMENTS
REAL Surface_Interval_Time
LOCAL VARIABLES
C-----
                                      !loop counter
   REAL Inspired_Helium_Pressure, Inspired Nitrogen Pressure
   REAL Initial Helium Pressure, Initial Nitrogen Pressure
   REAL HALDANE EQUATION
                                  !function subprogram
GLOBAL CONSTANTS IN NAMED COMMON BLOCKS
REAL Water Vapor Pressure
   COMMON /Block 8/ Water Vapor Pressure
GLOBAL VARIABLES IN NAMED COMMON BLOCKS
REAL Barometric Pressure
```

```
COMMON /Block 18/ Barometric Pressure
GLOBAL ARRAYS IN NAMED COMMON BLOCKS
REAL Helium Time Constant (16)
   COMMON /Block 1A/ Helium Time Constant
   REAL Nitrogen Time Constant (16)
   COMMON /Block 1B/ Nitrogen Time Constant
   REAL Helium Pressure (16), Nitrogen Pressure (16)
                                        !both input
   COMMON /Block 3/ Helium Pressure, Nitrogen Pressure
CALCULATIONS
Inspired Helium Pressure = 0.0
   Inspired Nitrogen Pressure = (Barometric Pressure -
        Water Vapor Pressure) *0.79
   DO I = 1,16
     Initial Helium Pressure = Helium Pressure(I)
     Initial Nitrogen Pressure = Nitrogen Pressure(I)
     Helium Pressure(I) = HALDANE EQUATION
      (Initial Helium Pressure, Inspired Helium Pressure,
     Helium_Time_Constant(I), Surface_Interval_Time)
     Nitrogen Pressure(I) = HALDANE EQUATION
     (Initial_Nitrogen_Pressure, Inspired_Nitrogen_Pressure,
     Nitrogen Time Constant(I), Surface Interval Time)
   END DO
END OF SUBROUTINE
END
SUBROUTINE VPM REPETITIVE ALGORITHM
   Purpose: This subprogram implements the VPM Repetitive Algorithm that was
   envisioned by Professor David E. Yount only months before his passing.
C-----
   SUBROUTINE VPM REPETITIVE ALGORITHM (Surface Interval Time)
   IMPLICIT NONE
ARGUMENTS
REAL Surface Interval Time
LOCAL VARIABLES
C-----
   INTEGER I
                                       !loop counter
   REAL Max Actual Gradient Pascals
   REAL Adj Crush Pressure He Pascals, Adj Crush Pressure N2 Pascals
   REAL Initial Allowable Grad He Pa, Initial Allowable Grad N2 Pa
   REAL New_Critical_Radius_He, New_Critical_Radius_N2
GLOBAL CONSTANTS IN NAMED COMMON BLOCKS
REAL Surface Tension Gamma, Skin Compression GammaC
   COMMON /Block 19/ Surface Tension Gamma, Skin Compression GammaC
```

```
REAL Regeneration_Time_Constant
    COMMON /Block 22/ Regeneration Time Constant
GLOBAL VARIABLES IN NAMED COMMON BLOCKS
REAL Units Factor
    COMMON /Block 16/ Units Factor
C-----
    GLOBAL ARRAYS IN NAMED COMMON BLOCKS
REAL Initial Critical Radius He(16)
    REAL Initial Critical Radius N2(16)
    COMMON /Block 6/ Initial Critical Radius He,
             Initial Critical Radius N2
    REAL Adjusted Critical Radius He(16)
                                                           !output
    REAL Adjusted Critical Radius N2 (16)
    COMMON /Block_7/ Adjusted_Critical_Radius_He,
                  Adjusted Critical Radius N2
    REAL Max Actual Gradient (16)
                                                           !input
    COMMON /Block 12/ Max Actual Gradient
    REAL Adjusted_Crushing_Pressure_He(16)
                                                           !input
    REAL Adjusted_Crushing_Pressure_N2(16)
    COMMON /Block_25/ Adjusted_Crushing_Pressure_He,
                   Adjusted Crushing Pressure N2
    REAL Initial Allowable Gradient He(16)
                                                           !input
    REAL Initial Allowable Gradient N2(16)
    COMMON /Block 27/
       Initial Allowable Gradient He, Initial Allowable Gradient N2
CALCULATIONS
DO I = 1,16
       Max Actual Gradient Pascals =
           (Max Actual Gradient(I)/Units Factor) * 101325.0
       Adj Crush Pressure He Pascals =
           (Adjusted Crushing Pressure He(I)/Units Factor) * 101325.0
       Adj Crush Pressure N2 Pascals =
           (Adjusted Crushing Pressure N2(I)/Units Factor) * 101325.0
        Initial Allowable Grad He Pa =
           (Initial Allowable Gradient He(I)/Units Factor) * 101325.0
        Initial Allowable Grad N2 Pa =
           (Initial Allowable Gradient N2(I)/Units Factor) * 101325.0
        IF (Max_Actual_Gradient(I)
                       .GT. Initial Allowable Gradient N2(I)) THEN
           New Critical Radius N2 = ((2.0*Surface Tension Gamma*
           (Skin Compression GammaC - Surface Tension Gamma))) /
           (Max Actual Gradient Pascals*Skin Compression GammaC -
           Surface Tension Gamma*Adj Crush Pressure N2 Pascals)
           Adjusted Critical Radius N2(I) =
           Initial Critical Radius N2(I) +
           (Initial Critical_Radius_N2(I)-New_Critical_Radius_N2)*
           EXP(-Surface Interval Time/Regeneration Time Constant)
        ELSE
```

```
Adjusted Critical Radius N2(I) =
         Initial Critical Radius N2(I)
      END IF
      IF (Max Actual Gradient(I)
                  .GT. Initial Allowable Gradient He(I)) THEN
         New Critical Radius He = ((2.0*Surface Tension Gamma*
         (Skin Compression GammaC - Surface Tension Gamma))) /
         (Max Actual Gradient Pascals*Skin Compression GammaC -
         Surface Tension Gamma*Adj Crush Pressure He Pascals)
         Adjusted Critical Radius He(I) =
         Initial Critical Radius He(I) +
         (Initial Critical Radius He(I)-New Critical Radius He)*
         EXP(-Surface_Interval_Time/Regeneration_Time_Constant)
      ELSE
         Adjusted Critical Radius He(I) =
         Initial Critical Radius He(I)
   END DO
END OF SUBROUTINE
RETURN
   END
SUBROUTINE CALC BAROMETRIC PRESSURE
C
   Purpose: This sub calculates barometric pressure at altitude based on the
C
   publication "U.S. Standard Atmosphere, 1976", U.S. Government Printing
C
   Office, Washington, D.C. The source for this code is a Fortran 90 program
C
   written by Ralph L. Carmichael (retired NASA researcher) and endorsed by
   the National Geophysical Data Center of the National Oceanic and
   Atmospheric Administration. It is available for download free from
   Public Domain Aeronautical Software at: http://www.pdas.com/atmos.htm
SUBROUTINE CALC BAROMETRIC PRESSURE (Altitude)
   IMPLICIT NONE
ARGUMENTS
REAL Altitude
LOCAL CONSTANTS
C-----
   REAL Radius of Earth, Acceleration of Gravity
   REAL Molecular_weight_of_Air, Gas_Constant_R
   REAL Temp_at_Sea_Level, Temp Gradient
   REAL Pressure at Sea Level Fsw, Pressure at Sea Level Msw
LOCAL VARIABLES
REAL Pressure at Sea Level, GMR Factor
   REAL Altitude Feet, Altitude Meters
   REAL Altitude Kilometers, Geopotential Altitude
   REAL Temp at Geopotential Altitude
GLOBAL VARIABLES IN NAMED COMMON BLOCKS
LOGICAL Units Equal Fsw, Units Equal Msw
```

```
COMMON /Block_15/ Units_Equal_Fsw, Units_Equal_Msw
    REAL Barometric Pressure
                                                         !output
    COMMON /Block 18/ Barometric Pressure
CALCULATIONS
Radius of Earth = 6369.0
                                                     !kilometers
    Acceleration of Gravity = 9.80665
                                                 !meters/second^2
    Molecular weight of Air = 28.9644
                                                          !mols
    Gas Constant R = 8.31432
                                            !Joules/mol*deg Kelvin
    Temp at Sea Level = 288.15
                                                  !degrees Kelvin
    Pressure at Sea Level Fsw = 33.0 !feet of seawater based on 101325 Pa
                                  !at sea level (Standard Atmosphere)
    Pressure at Sea Level Msw = 10.0 !meters of seawater based on 100000 Pa
                                      !at sea level (European System)
    Temp Gradient = -6.5
                                      !Change in Temp deg Kelvin with
                                    !change in geopotential altitude,
                                  !valid for first layer of atmosphere
                                   !up to 11 kilometers or 36,000 feet
    GMR Factor = Acceleration of Gravity *
              Molecular weight of Air / Gas Constant R
    IF (Units Equal Fsw) THEN
       Altitude Feet = Altitude
       Altitude Kilometers = Altitude Feet / 3280.839895
       Pressure at Sea Level = Pressure at Sea Level Fsw
    END IF
    IF (Units Equal Msw) THEN
       Altitude Meters = Altitude
       Altitude Kilometers = Altitude Meters / 1000.0
       Pressure at Sea Level = Pressure at Sea Level Msw
    END IF
    Geopotential_Altitude = (Altitude_Kilometers * Radius_of_Earth) /
                        (Altitude Kilometers + Radius of Earth)
    Temp at Geopotential Altitude = Temp at Sea Level
               + Temp_Gradient * Geopotential_Altitude
    Barometric_Pressure = Pressure_at_Sea_Level *

* EXP(ALOG(Temp_at_Sea_Level / Temp_at_Geopotential_Altitude) *
       GMR_Factor / Temp_Gradient)
END OF SUBROUTINE
RETURN
    END
SUBROUTINE VPM ALTITUDE DIVE ALGORITHM
    Purpose: This subprogram updates gas loadings and adjusts critical radii
    (as required) based on whether or not diver is acclimatized at altitude or
C
    makes an ascent to altitude before the dive.
SUBROUTINE VPM ALTITUDE DIVE ALGORITHM
    IMPLICIT NONE
```

```
LOCAL VARIABLES
CHARACTER Diver_Acclimatized_at_Altitude*3, OS Command*3
    INTEGER I
                                                    !loop counter
    LOGICAL Diver Acclimatized
    REAL Altitude of Dive, Starting Acclimatized Altitude
    REAL Ascent to Altitude Hours, Hours at Altitude Before Dive
    REAL Ascent to Altitude Time, Time at Altitude Before Dive
    REAL Starting Ambient Pressure, Ending Ambient Pressure
    REAL Initial Inspired N2 Pressure, Rate, Nitrogen Rate
    REAL Inspired Nitrogen Pressure, Initial Nitrogen Pressure
    REAL Compartment Gradient, Compartment Gradient Pascals
    REAL Gradient_He_Bubble_Formation, Gradient_N2_Bubble_Formation
    REAL New Critical Radius He, New Critical Radius N2
    REAL Ending_Radius_He, Ending_Radius_N2
    REAL Regenerated Radius He, Regenerated Radius N2
    REAL HALDANE EQUATION
                                               !function subprogram
    REAL SCHREINER EQUATION
                                               !function subprogram
GLOBAL CONSTANTS IN NAMED COMMON BLOCKS
REAL Water Vapor Pressure
    COMMON /Block 8/ Water Vapor Pressure
    REAL Constant Pressure Other Gases
    COMMON /Block 17/ Constant Pressure Other Gases
    REAL Surface Tension Gamma, Skin Compression GammaC
    COMMON /Block 19/ Surface Tension Gamma, Skin Compression GammaC
    REAL Regeneration Time Constant
    COMMON /Block 22/ Regeneration Time Constant
GLOBAL VARIABLES IN NAMED COMMON BLOCKS
LOGICAL Units Equal Fsw, Units Equal Msw
    COMMON /Block 15/ Units Equal Fsw, Units Equal Msw
    REAL Units Factor
    COMMON /Block_16/ Units_Factor
    REAL Barometric Pressure
    COMMON /Block 18/ Barometric Pressure
C-----
    GLOBAL ARRAYS IN NAMED COMMON BLOCKS
REAL Nitrogen Time Constant (16)
    COMMON /Block 1B/ Nitrogen Time Constant
    REAL Helium Pressure (16), Nitrogen Pressure (16)
                                                     !both input
    COMMON /Block 3/ Helium Pressure, Nitrogen Pressure
                                                     !and output
    REAL Initial Critical Radius He(16)
                                                      !both input
    REAL Initial Critical Radius N2(16)
                                                      !and output
    COMMON /Block 6/ Initial Critical Radius He,
             Initial Critical Radius N2
    REAL Adjusted Critical Radius He (16)
                                                         !output
```

```
REAL Adjusted Critical Radius N2(16)
    COMMON /Block_7/ Adjusted_Critical Radius He,
                   Adjusted_Critical Radius N2
NAMELIST FOR PROGRAM SETTINGS (READ IN FROM ASCII TEXT FILE)
NAMELIST /Altitude Dive Settings/ Altitude of Dive,
           Diver Acclimatized at_Altitude,
            Starting Acclimatized Altitude, Ascent to Altitude Hours,
            Hours at Altitude Before Dive
OS Command = 'CLS'
    OPEN (UNIT = 12, FILE = 'ALTITUDE.SET', STATUS = 'UNKNOWN',
            ACCESS = 'SEQUENTIAL', FORM = 'FORMATTED')
     READ (12, Altitude Dive Settings)
     IF ((Units Equal Fsw) .AND. (Altitude of Dive .GT. 30000.0)) THEN
        CALL SYSTEMQQ (OS Command)
        WRITE (*,900)
        WRITE (*,901)
        STOP 'PROGRAM TERMINATED'
     END IF
     IF ((Units_Equal_Msw) .AND. (Altitude_of Dive .GT. 9144.0)) THEN
        CALL SYSTEMQQ (OS Command)
        WRITE (*,900)
        WRITE (*,901)
        STOP 'PROGRAM TERMINATED'
     END IF
     IF ((Diver_Acclimatized at Altitude .EQ. 'YES') .OR.
                   (Diver Acclimatized at Altitude .EQ. 'yes')) THEN
        Diver Acclimatized = (.TRUE.)
     ELSE IF ((Diver Acclimatized at Altitude .EQ. 'NO') .OR.
                    (Diver Acclimatized at Altitude .EQ. 'no')) THEN
        Diver Acclimatized = (.FALSE.)
     ELSE
        CALL SYSTEMQQ (OS Command)
        WRITE (*,902)
        WRITE (*,901)
        STOP 'PROGRAM TERMINATED'
     END IF
     Ascent_to_Altitude_Time = Ascent_to_Altitude_Hours * 60.0
     Time_at_Altitude_Before_Dive = Hours_at_Altitude_Before_Dive*60.0
     IF (Diver Acclimatized) THEN
        CALL CALC BAROMETRIC PRESSURE (Altitude of Dive)
                                                           !subroutine
        WRITE (*,802) Altitude of Dive, Barometric Pressure
        DO I = 1,16
        Adjusted Critical Radius N2(I) = Initial Critical Radius N2(I)
        Adjusted Critical Radius He(I) = Initial Critical Radius He(I)
        Helium Pressure(I) = 0.0
        Nitrogen Pressure(I) = (Barometric Pressure -
            Water Vapor Pressure) *0.79
        END DO
    ELSE
        IF ((Starting Acclimatized Altitude .GE. Altitude of Dive)
                 .OR. (Starting Acclimatized Altitude .LT. 0.0)) THEN
            CALL SYSTEMQQ (OS Command)
            WRITE (*,903)
```

```
WRITE (*,904)
    WRITE (*,901)
    STOP 'PROGRAM TERMINATED'
END IF
CALL CALC_BAROMETRIC PRESSURE
                                                            !subroutine
                   (Starting_Acclimatized_Altitude)
Starting Ambient Pressure = Barometric Pressure
DO I = 1,16
Helium Pressure(I) = 0.0
Nitrogen Pressure(I) = (Barometric Pressure -
    Water Vapor Pressure) *0.79
CALL CALC BAROMETRIC PRESSURE (Altitude of Dive)
                                                            !subroutine
WRITE (*,802) Altitude of Dive, Barometric Pressure
Ending Ambient Pressure = Barometric Pressure
Initial_Inspired_N2_Pressure = (Starting_Ambient_Pressure
           - Water Vapor Pressure) *0.79
Rate = (Ending_Ambient_Pressure - Starting_Ambient_Pressure)
        / Ascent to Altitude Time
Nitrogen Rate = Rate*0.79
DO I = 1,16
    Initial_Nitrogen_Pressure = Nitrogen_Pressure(I)
   Nitrogen Pressure(I) = SCHREINER EQUATION
        (Initial_Inspired_N2_Pressure, Nitrogen_Rate,
        Ascent to Altitude Time, Nitrogen Time Constant(I),
        Initial Nitrogen Pressure)
    Compartment Gradient = (Nitrogen Pressure(I)
        + Constant Pressure Other Gases)
        - Ending Ambient Pressure
    Compartment Gradient Pascals =
        (Compartment Gradient / Units Factor) * 101325.0
    Gradient He Bubble Formation =
    ((2.0*Surface Tension Gamma*
    (Skin Compression GammaC - Surface Tension Gamma)) /
    (Initial Critical Radius He(I)*Skin Compression GammaC))
    IF (Compartment Gradient Pascals .GT.
                            Gradient_He_Bubble_Formation) THEN
        New_Critical_Radius_He = ((2.0*Surface_Tension_Gamma*
        (Skin_Compression_GammaC - Surface_Tension_Gamma))) /
        (Compartment Gradient Pascals*Skin Compression GammaC)
        Adjusted Critical Radius He(I) =
        Initial Critical Radius He(I) +
        (Initial_Critical_Radius_He(I)-
        New Critical Radius He) *
        EXP(-Time at Altitude Before Dive/
        Regeneration Time Constant)
        Initial Critical Radius He(I) =
        Adjusted Critical Radius He(I)
        Ending Radius He = 1.0/(Compartment Gradient Pascals/
        (2.0*(Surface Tension Gamma-Skin Compression GammaC))
        + 1.0/Initial Critical Radius He(I))
        Regenerated Radius He =
        Initial Critical Radius He(I) +
```

```
(Ending Radius He - Initial Critical Radius He(I)) *
                 EXP(-Time_at_Altitude Before Dive/
                 Regeneration_Time_Constant)
                 Initial Critical Radius He(I) =
                 Regenerated Radius He
                 Adjusted Critical Radius He(I) =
                 Initial Critical Radius He(I)
             END IF
             Gradient N2 Bubble Formation =
             ((2.0*Surface Tension Gamma*
             (Skin Compression GammaC - Surface Tension Gamma)) /
             (Initial Critical Radius N2(I)*Skin Compression GammaC))
             IF (Compartment Gradient Pascals .GT.
                                     Gradient_N2_Bubble_Formation) THEN
                 New Critical Radius N2 = ((2.0*Surface Tension Gamma*
                 (Skin Compression_GammaC - Surface_Tension_Gamma))) /
                 (Compartment Gradient Pascals*Skin Compression GammaC)
                 Adjusted_Critical_Radius_N2(I) =
                 Initial_Critical_Radius_N2(I) +
                 (Initial_Critical_Radius_N2(I)-
                 New Critical Radius N2)*
                 EXP(-Time_at_Altitude_Before_Dive/
                 Regeneration Time Constant)
                 Initial Critical Radius N2(I) =
                 Adjusted Critical Radius N2(I)
             ELSE
                 Ending Radius N2 = 1.0/(Compartment Gradient Pascals/
                 (2.0*(Surface Tension Gamma-Skin Compression_GammaC))
                 + 1.0/Initial_Critical_Radius_N2(I))
                 Regenerated Radius N2 =
                 Initial Critical Radius N2(I) +
                 (Ending Radius N2 - Initial Critical Radius N2(I)) *
                 EXP(-Time at Altitude Before Dive/
                 Regeneration Time Constant)
                 Initial Critical Radius N2(I) =
                 Regenerated_Radius_N2
                 Adjusted_Critical_Radius_N2(I) =
                 Initial_Critical_Radius_N2(I)
             END IF
         END DO
         Inspired Nitrogen Pressure = (Barometric Pressure -
         Water Vapor_Pressure) *0.79
         DO I = 1,16
             Initial Nitrogen Pressure = Nitrogen Pressure(I)
             Nitrogen Pressure(I) = HALDANE EQUATION
             (Initial_Nitrogen_Pressure, Inspired Nitrogen Pressure,
             Nitrogen_Time_Constant(I), Time_at_Altitude_Before_Dive)
         END DO
     END IF
     CLOSE (UNIT = 12, STATUS = 'KEEP')
     RETURN
FORMAT STATEMENTS - PROGRAM OUTPUT
```

```
FORMAT ('OALTITUDE = ',1X,F7.1,4X,'BAROMETRIC PRESSURE = ',
  *F6.3)
FORMAT STATEMENTS - ERROR MESSAGES
FORMAT ('0ERROR! ALTITUDE OF DIVE HIGHER THAN MOUNT EVEREST')
  FORMAT ('')
901
  FORMAT ('OERROR! DIVER ACCLIMATIZED AT ALTITUDE',
902
  *1X,'MUST BE YES OR NO')
903
  FORMAT ('OERROR! STARTING ACCLIMATIZED ALTITUDE MUST BE LESS',
  *1X, 'THAN ALTITUDE OF DIVE')
  FORMAT (' AND GREATER THAN OR EQUAL TO ZERO')
END OF SUBROUTINE
SUBROUTINE CLOCK
C
  Purpose: This subprogram retrieves clock information from the Microsoft
C
  operating system so that date and time stamp can be included on program
  output.
SUBROUTINE CLOCK (Year, Month, Day, Clock Hour, Minute, M)
  IMPLICIT NONE
C-----
  ARGUMENTS
CHARACTER M*1
  INTEGER*2 Month, Day, Year
  INTEGER*2 Minute, Clock Hour
LOCAL VARIABLES
INTEGER*2 Hour, Second, Hundredth
CALCULATIONS
CALL GETDAT (Year, Month, Day)
                            !Microsoft run-time
  CALL GETTIM (Hour, Minute, Second, Hundredth)
                               !subroutines
  IF (Hour .GT. 12) THEN
    Clock Hour = Hour - 12
    'q' = M
  ELSE
    Clock Hour = Hour
    M = 'a'
  ENDIF
C-----
  END OF SUBROUTINE
END
```